
Power System Services of PV-systems: Requirements, testing and application in Germany

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Power System Services of PV-systems: Requirements, testing and application in Germany

- Introduction
- Power System Services of PV-systems
 - Grid code requirements
 - Test procedures for PV-systems
- Application of power system services
 - Voltage control by reactive power
 - Voltage control by active network components
- Conclusions

1. Introduction

Generating capacities in Germany

■ Generation capacity in Germany

- 137.5 GW (in 2009) in total

- 46 GW of RES

■ Wind

- Increase since 1994

- 25 GW in 2009

■ PV

- Increase since 2004

- 17.3 GW in 2010

- 52 GW in 2020¹

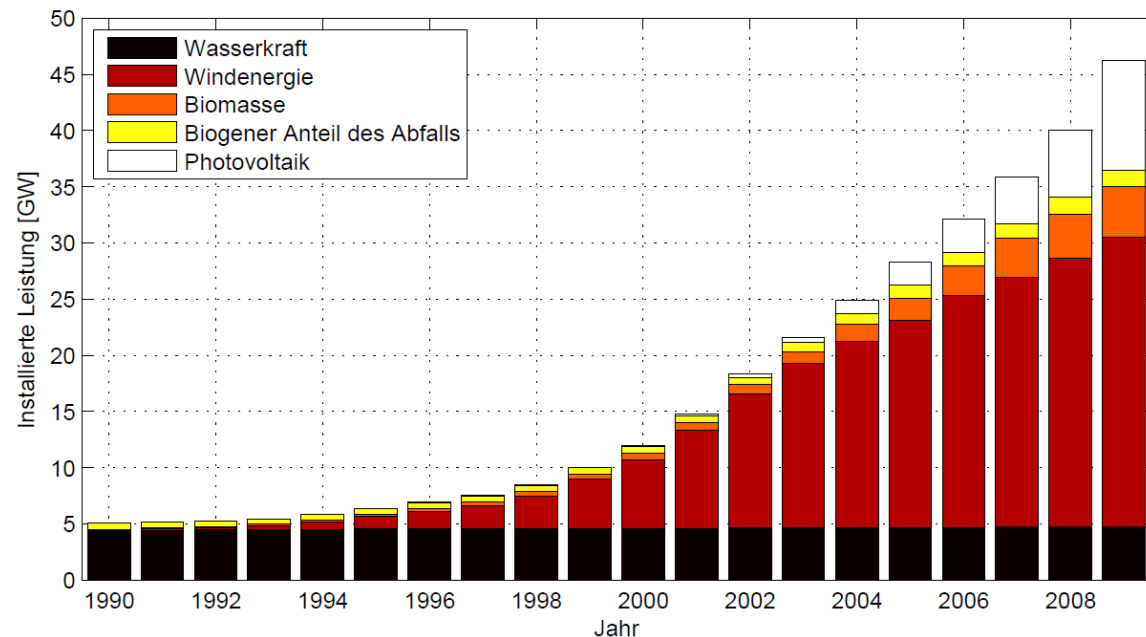


Diagram: Fraunhofer IWES, Data: Erneuerbare Energien in Zahlen, BMU, 2010

¹: National development plan for renewable energies

1. Introduction

Interconnection of PV-systems

- Interconnection of PV-systems mainly to LV due to power ratings
- Interconnected of PV-systems to HV or MV
 - $\approx 18\%$ ¹ (end of 2008)
- Jan. 2009 to Sept. 2010
 - 9335 MW_p new installed PV-power
 - Share of PV-systems with rated power > 100kWp: 3278 MWp
- Grid integration of PV on distribution system level

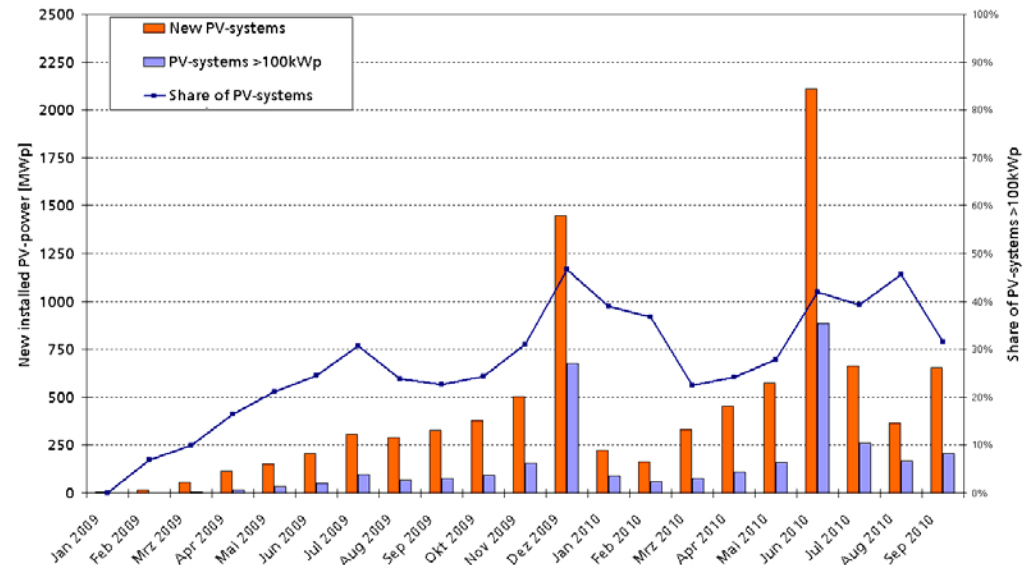


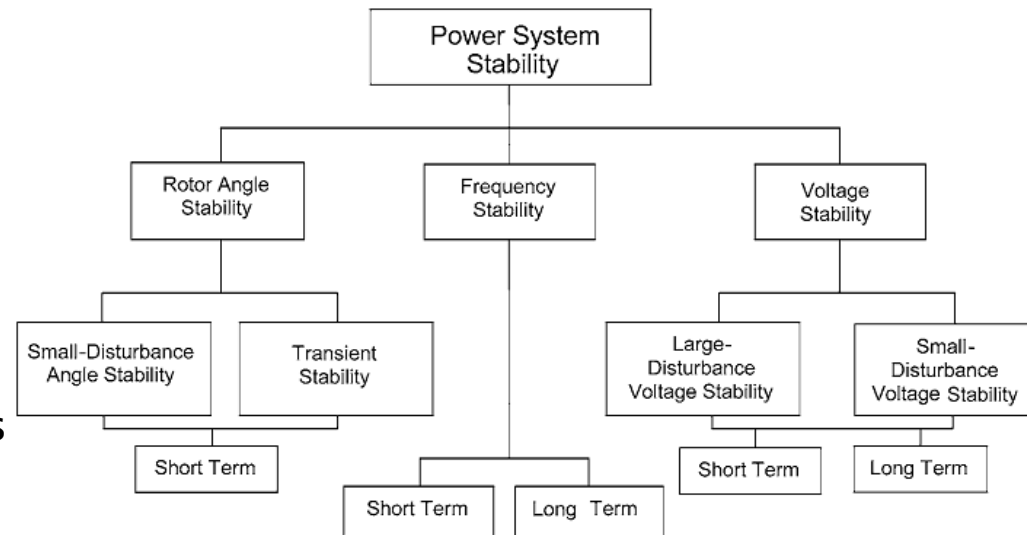
Diagram: Fraunhofer IWES; Data: Information of new installed PV-systems of BNetzA

¹EEG Statistikbericht 2008; BNetzA

1. Introduction

Grid integration constraints

- Power System Stability
 - Rotor angle stability
 - Frequency stability
 - Voltage stability
- Network Constraints
 - Capacity of lines, cables, transformers
 - Power quality
 - Steady-state voltage limits
 - Harmonics
 - Flicker
 - ...



Source: Definition and Classification of Power System Stability, IEEE/CIGRE Joint Task Force on Stability Terms and Definitions, IEEE Transactions on Power Systems, Prabha Kundur et. al.

1. Introduction

Grid integration challenges and approaches

■ Transmission network (HV/EHV)

■ Challenges

- Power generation not located to load centers
- Integration of offshore wind parks

■ Approaches

- Grid reinforcement
- Power System Services of DER units
- Central storages
- FACTS

■ Distribution network (MV/LV)

■ Challenges

- Bidirectional power flows
- Voltage control

■ Approaches

- Power System Services of DER units
- Active network components
- Manageability of loads
- Local storages
- Grid reinforcement

2. Power System Services of PV-systems Grid code requirements – Overview

- Pre-condition for connection
 - Fulfilling of technical minimum standards concerning electrical behaviour (§6 EEG)
 - Link to grid codes
 - Approval of Conformity by certificates (§64 EEG)
- Grid codes in Germany
 - Describe behaviour of DER units in order to meet system needs
 - High voltage / Extra high voltage
 - [Transmission Code 2007](#)
 - Medium voltage
 - [BDEW MV-guideline](#)
 - Low voltage
 - [E VDE-AR-N 4105](#) (Draft version)



2. Power System Services of PV-systems Grid code requirements – Overview

- Distribution code „DER plants connected MV distribution grid“
 - Technical requirements for DER plants (steady state / transient)
 - Basic procedure for approval of conformity
- Link to Technical Guidelines of FGW for verification of requested electrical behaviour
 - FGW TR3: Testing procedures
 - Link to IEC 61400-21
 - Adaptation of test procedures for PV
 - FGW TR4: Modelling
 - FGW TR8: Certification



2. Power System Services of PV-systems

Grid code requirements – Overview

■ Static requirements

- Limitation of power-quality characteristic parameters
 - Harmonics, interharmonics and higher frequency components
 - Flicker
 - Switching operation
- Active power control
 - Active power reduction by network operator
 - Active power reduction at over-frequency
- Reactive power control

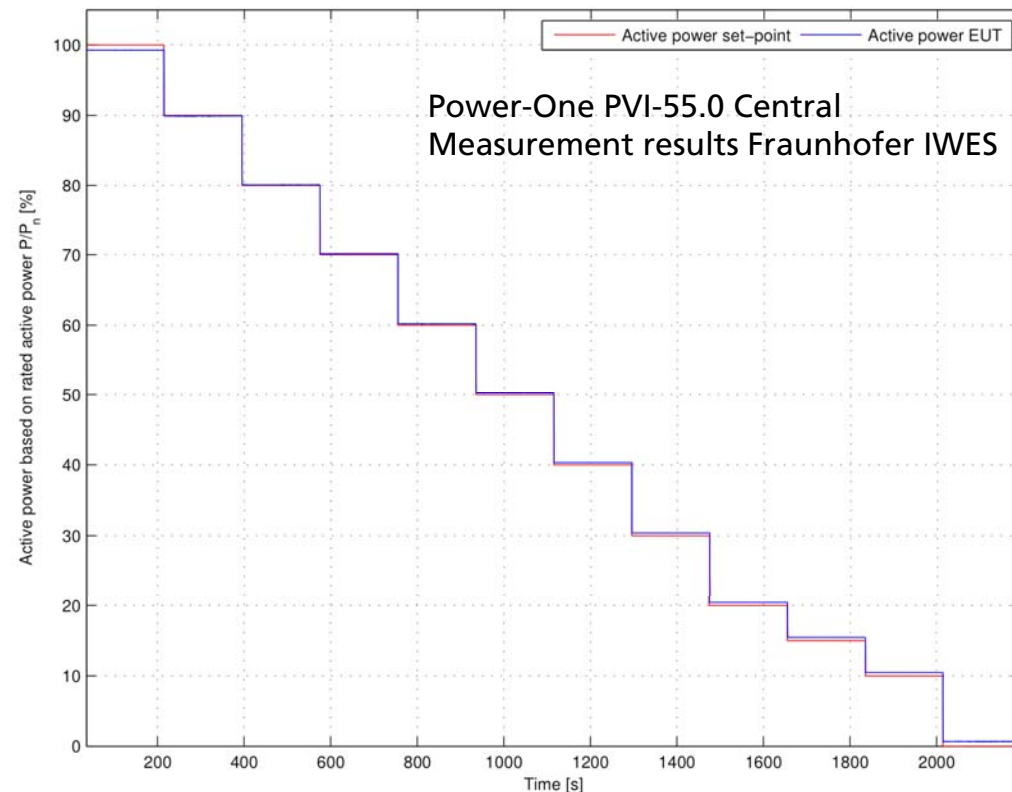
■ Dynamic requirements

- Fault-ride-through (FRT) capability with no disconnection of DER plants during the voltage dip
- No change of active power generation after faults
- Feed-in of reactive power during the fault for voltage stabilization
- Limitation of short-circuit current

2. Power System Services of PV-systems

Grid code requirements – Active power control

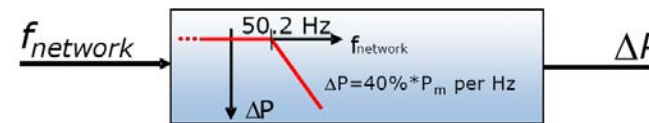
- Grid safety management
 - In case of danger for grid operation / overloading of network equipment
- Network operator is allowed to reduce active power remotely
- Unit / plant must technically be able to reduce active power in steps of $\leq 10\% P_n$
- Common power reduction levels are 100%, 60%, 30% and 0%
- Response time of 1 minute at most



2. Power System Services of PV-systems

Grid code requirements – Active power control

- Automatic active power reduction depending on grid frequency
- Grid support in case of power surplus
- Avoiding grid instabilities due to immediate disconnection of large generation capacities
- Under normal grid conditions no impact on energy yield
- For inverter no additional hardware required



$$\Delta P = 20 P_m \frac{50.2 \text{ Hz} - f_{\text{network}}}{50 \text{ Hz}} \quad \text{at } 50.2 \text{ Hz} < f_{\text{network}} < 51.5 \text{ Hz}$$

P_m instantaneously available power

ΔP power reduction

f_{network} network frequency

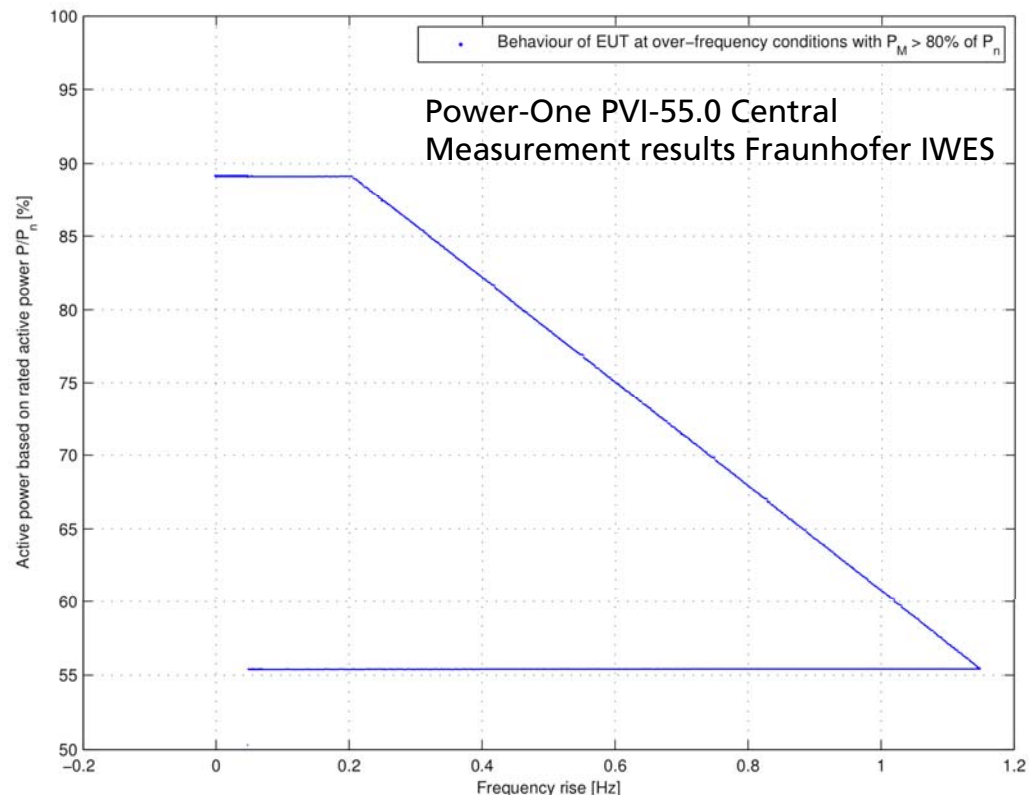
within the range of $47.5 \text{ Hz} < f_{\text{network}} \leq 50.2 \text{ Hz}$ no limitation

at $f_{\text{network}} \leq 47.5 \text{ Hz}$ and $f_{\text{network}} \geq 51.5 \text{ Hz}$ disconnection from the grid

2. Power System Services of PV-systems

Grid code requirements – Active power control

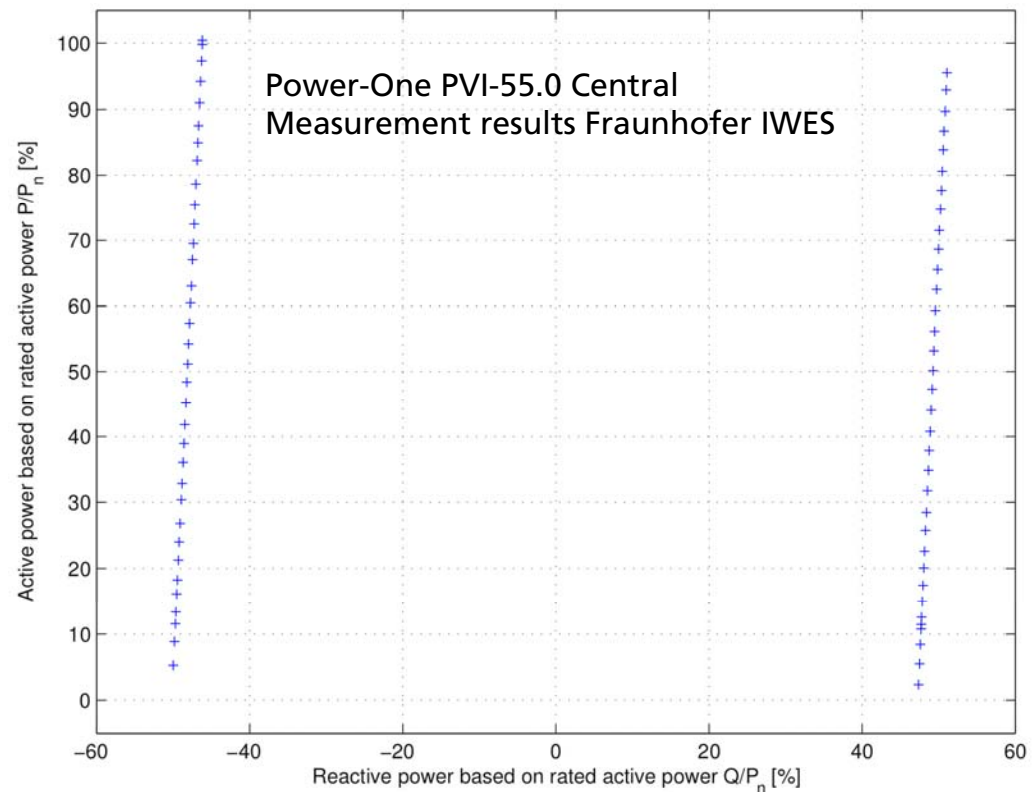
- Measurement results of a Power-One PVI-55.0 Central inverter at Fraunhofer IWES
- Start of reduction at $f_{\text{Grid}} > 50.20 \text{ Hz}$
- Instantaneously available power at 50.20Hz is used for active power reduction calculations
- Amount of active power reduction is determined by droop with of 40% per Hz
- Internal „hysteresis“: Rise of active power if $f_{\text{grid}} \leq 50.05 \text{ Hz}$



2. Power System Services of PV-systems

Grid code requirements – Reactive power capability

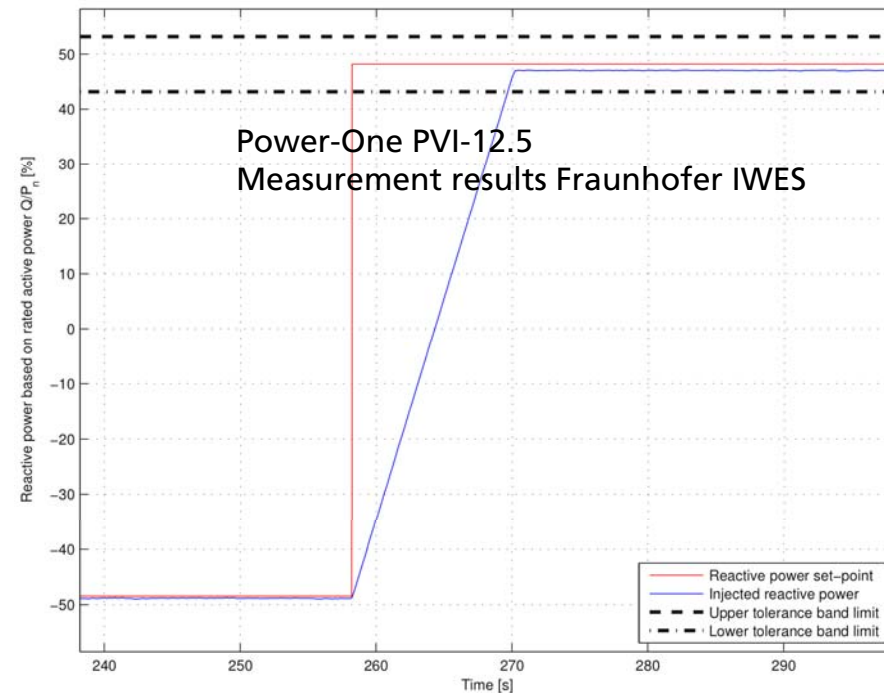
- Maintenance of grid voltage
- Generating unit must be able to provide reactive power during normal operation
- Required power factor $\cos \varphi$ at network connection point of plant:
 - 0.95_{underexcited} to 0.95_{overexcited}
- Impact on inverter design
 - Apparent power has to be increased



2. Power System Services of PV-systems

Grid code requirements – Reactive power capability

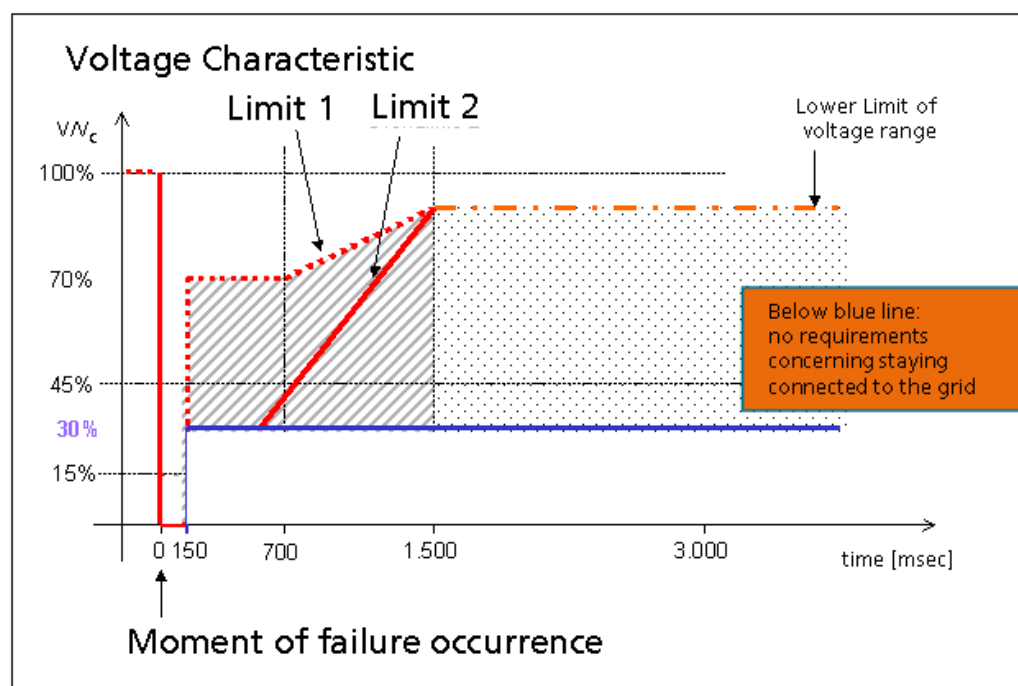
- Reactive power set-point provision
 - Fixed set-point for Q or power factor $\cos \varphi$
 - Variable set-point for Q or power factor $\cos \varphi$ provided remotely by network operator
 - Characteristic curve
 - $\cos \varphi$ (P) droop
 - Q(U) droop
- Response times
 - Variable set-points: few minutes
 - Characteristic curves
 - 10s to 1 min



2. Power System Services of PV-systems

Grid code requirements – Fault-Ride-Through (FRT)

- Generating units must stay connected during grid faults
- Different FRT-curves
 - Type 1: Direct coupled synchronous generators
 - Type 2: all other generating units
- Requested behaviour of generating unit depends on mainly two factors:
 - Depth of voltage dip
 - Duration of voltage dip
- Behaviour of unit:
 - Stay connected during fault
 - Short time disconnection with resynchronisation within 2s at most
 - Reactive current injection + short time disconnection
 - No requirements

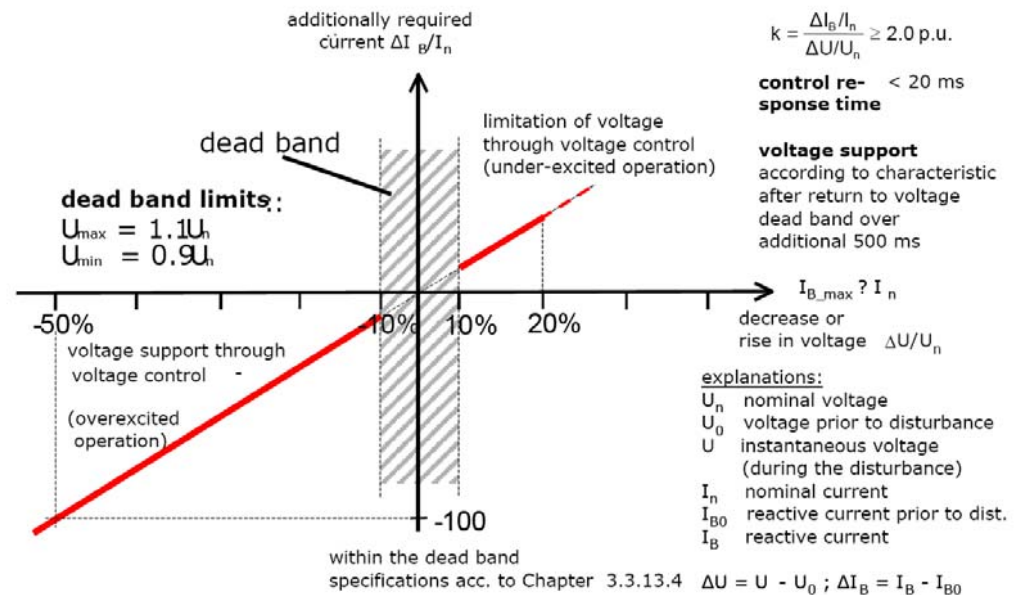


Source: Erzeugungsanlagen am Mittelspannungsnetz. BDEW, Release June 2008

2. Power System Services of PV-systems

Grid code requirements – Fault-Ride-Through (FRT)

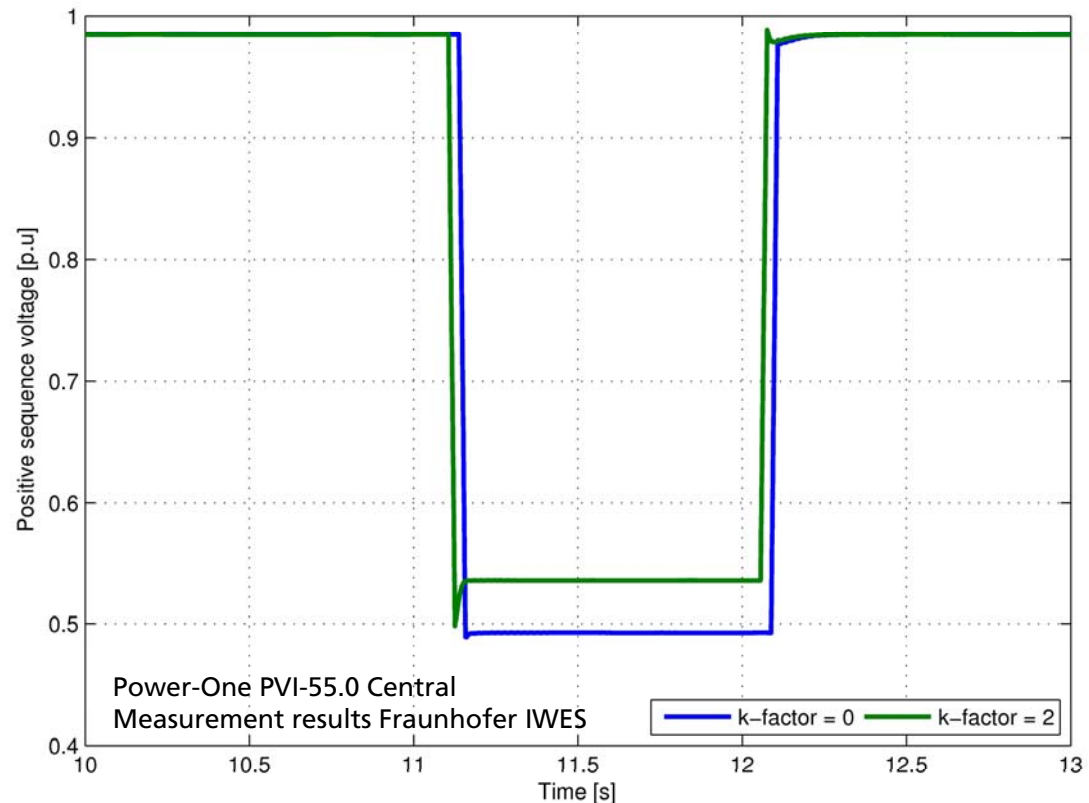
- Reactive current injection of unit according to Transmission Code 2007
- Amount of reactive power is determined by k-factor
 - $k = \Delta I_B / I_n / \Delta U / U_n$
 - Depth of grid fault
 - Reactive current before fault
 - Voltage before fault
- Response time ≤ 20 ms
- Max. reactive current: $I_B \leq 1.0 I_n$
- Max. duration of reactive current injection: time of fault clearing + 500ms
- In terms of unsymmetrical faults a release of overvoltage protection has to be avoided



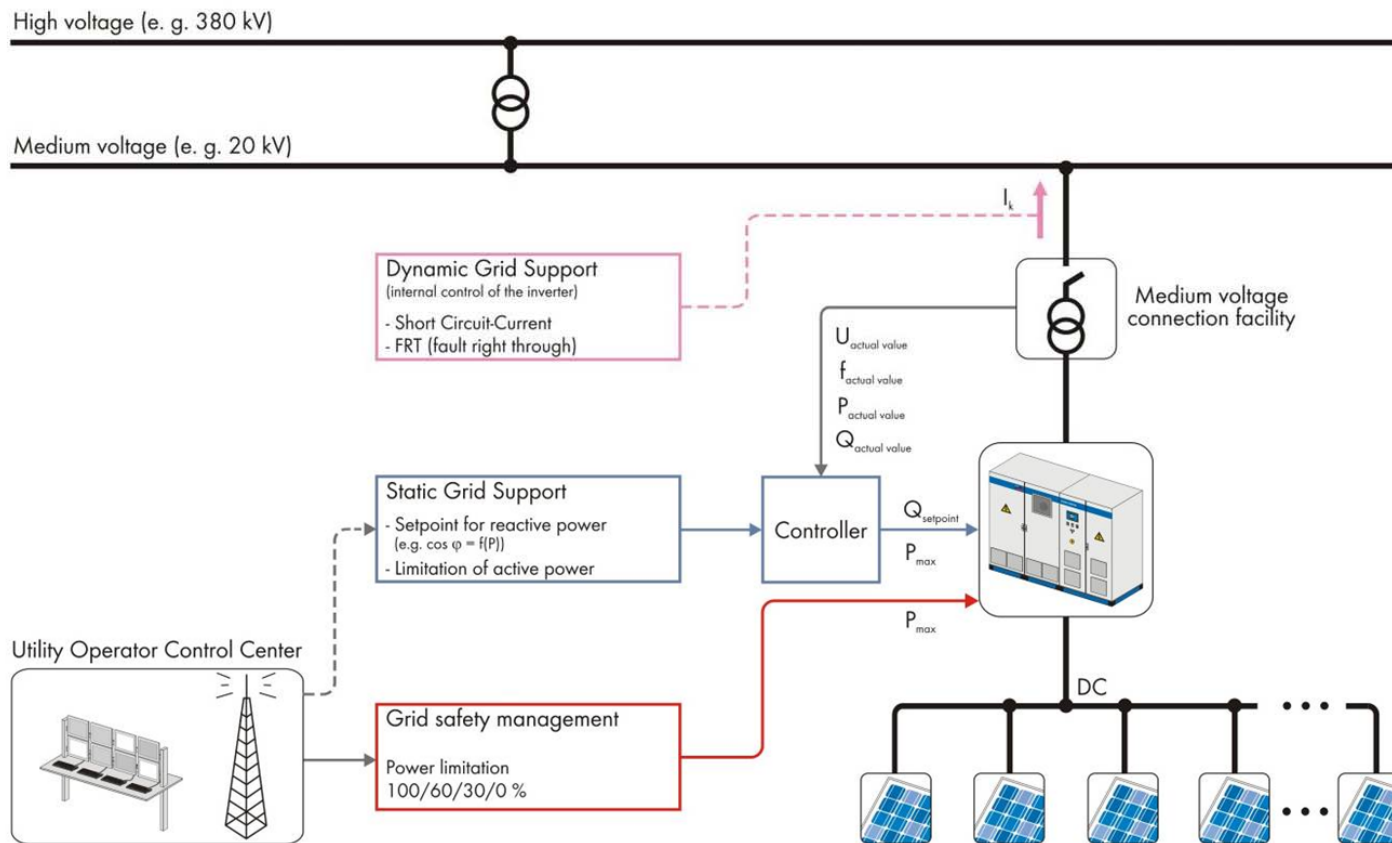
2. Power System Services of PV-systems

Grid code requirements – Fault-Ride-Through (FRT)

- Influence of reactive current on grid voltage during fault
- For both cases the same voltage dip is used
 - k-factor 0: no reactive current
 - k-factor 2: due to reactive current voltage is raised



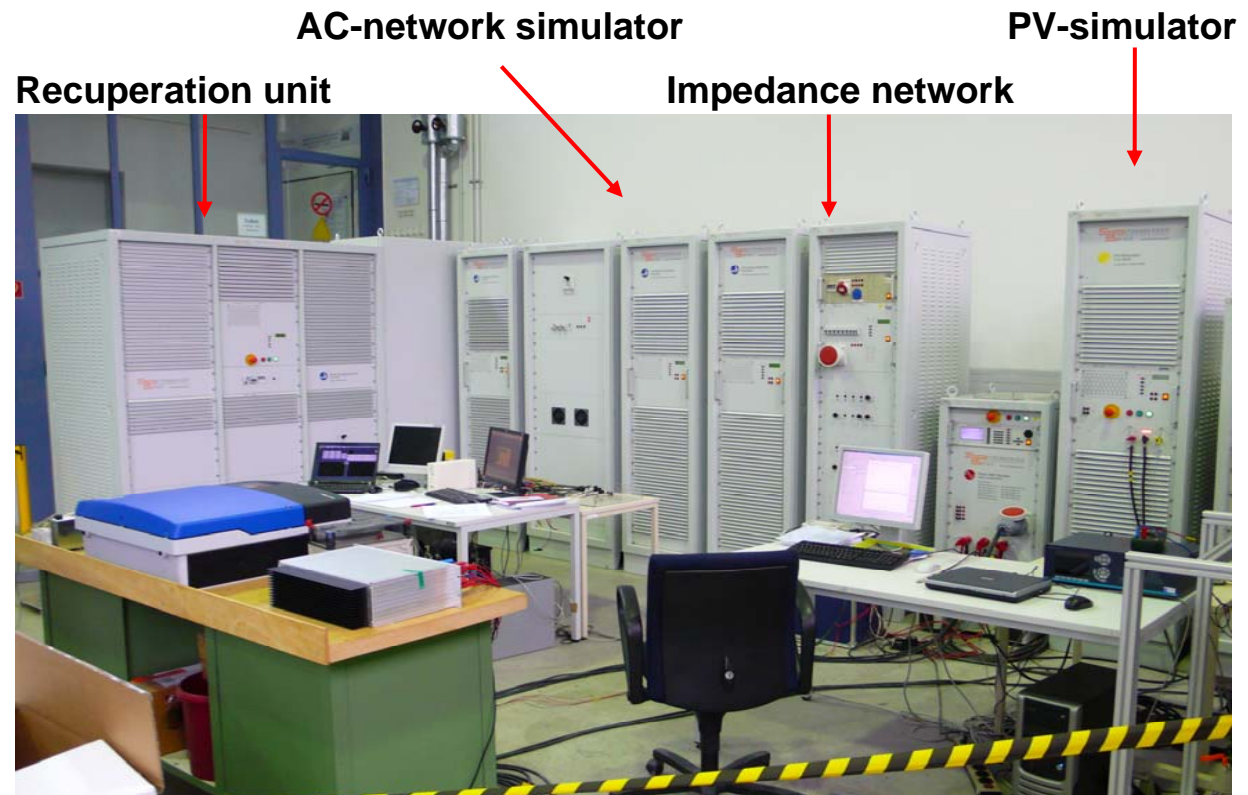
2. Power System Services of PV-systems Grid code requirements – Implementation



2. Power System Services of PV-systems

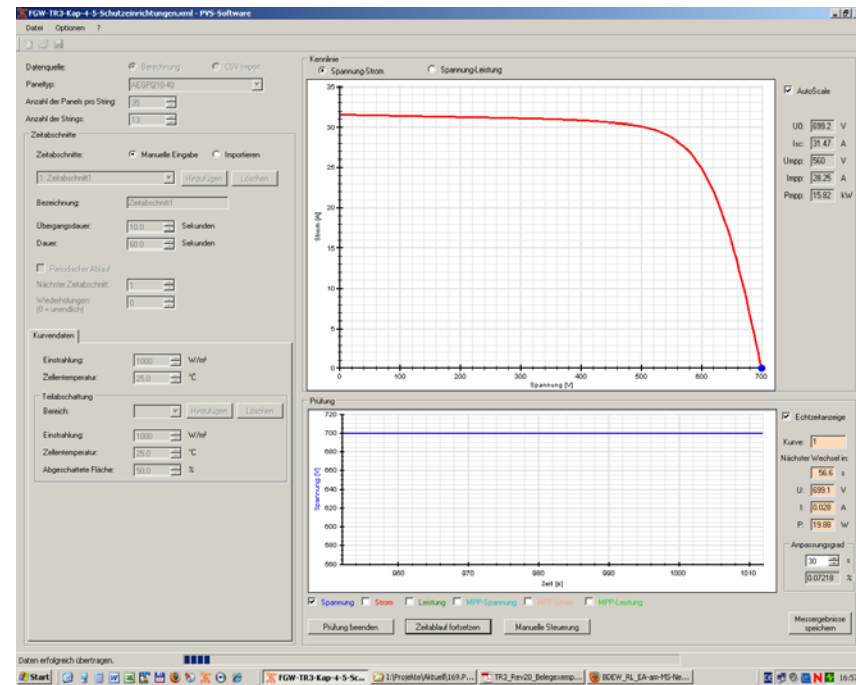
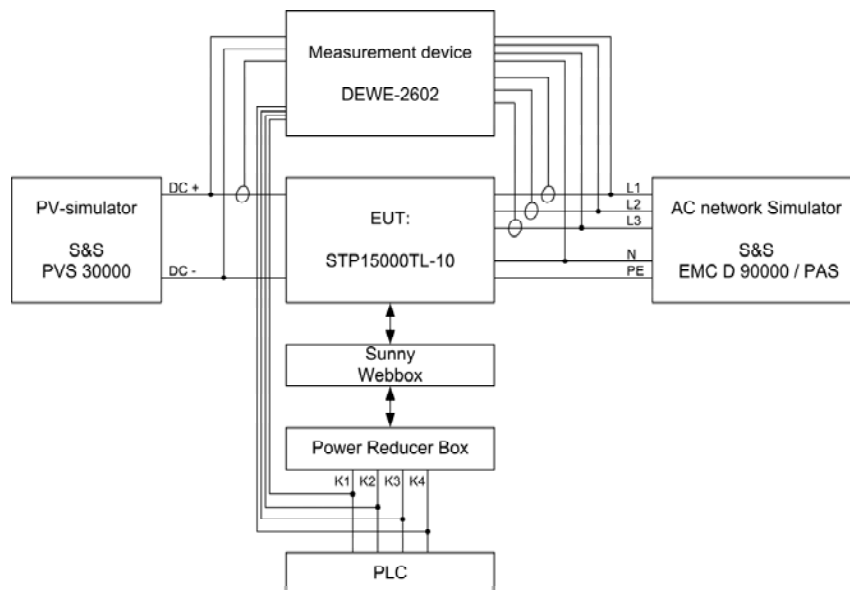
Test procedures for PV-systems – Testing environments

- AC-network simulator with additional impedance network
 - 90 kVA
 - Linear amplifiers
 - 4-quadrant operation
- PV-simulator 30kW
- Special testing equipment for PV-systems with higher power ratings



2. Power System Services of PV-systems

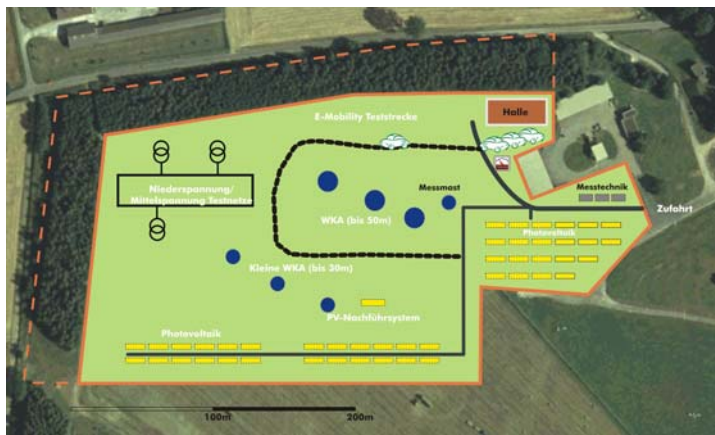
Test procedures for PV-systems – Testing environments



2. Power System Services of PV-systems

Test procedures for PV-systems – Testing environments

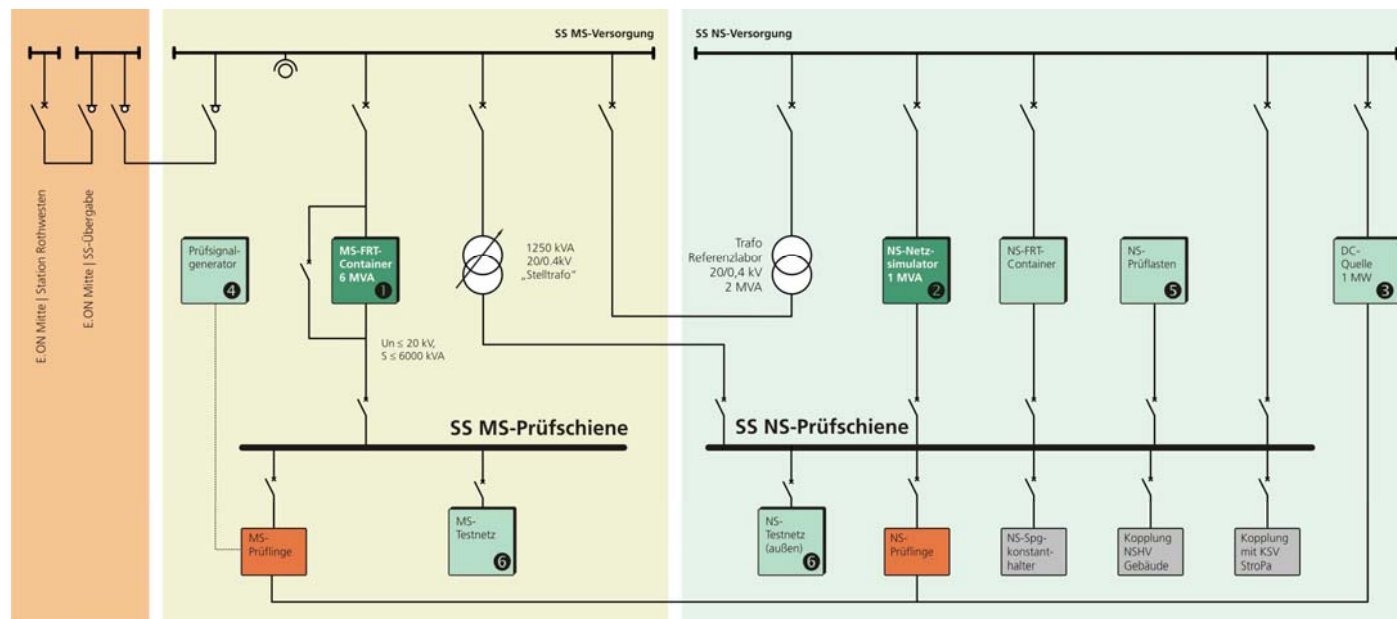
- SysTec
 - Experimental hall with 600m²
 - Testing environment for high power converters and network components
 - Testing environment for grid integration of E-Mobility



2. Power System Services of PV-systems

Test procedures for PV-systems – Testing environments

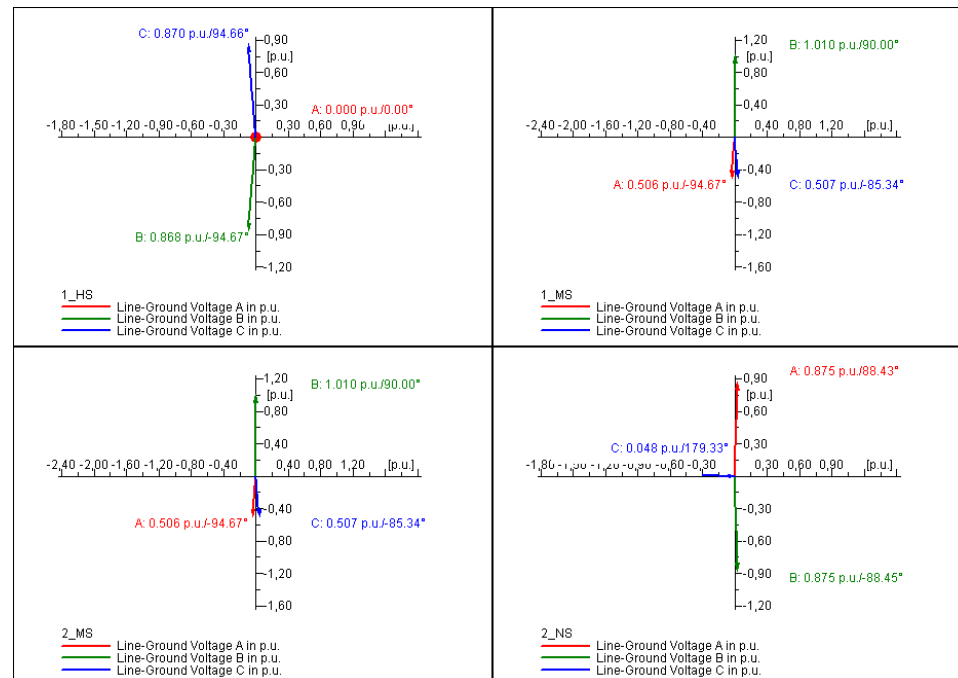
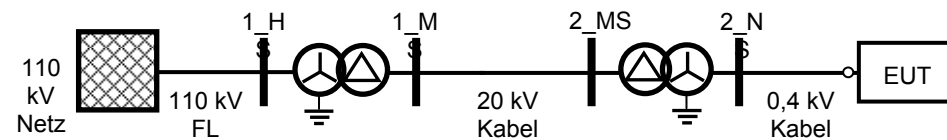
- 6 MVA FRT-container (MV)
- 1 MVA AC-network simulator (LV)
- 1 MW DC-source
- Signal generator
- Loads (resistive, inductive, capacitive)
- LV and MV test networks



2. Power System Services of PV-systems

Test procedures for PV-systems – Testing procedures

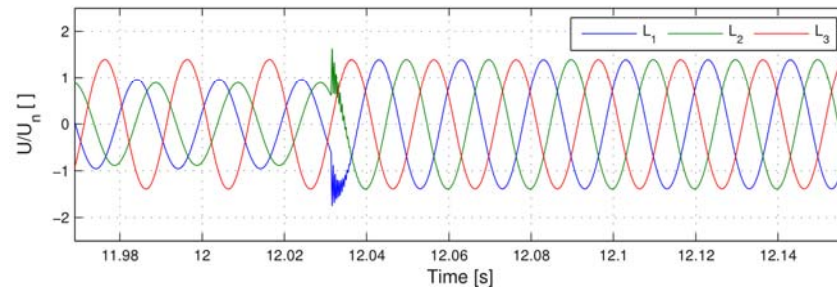
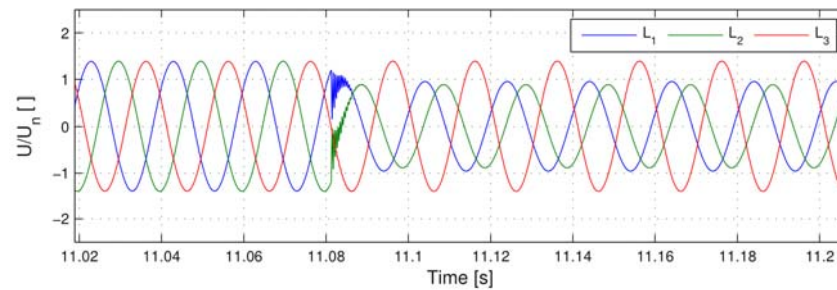
- Test of behaviour of DER units during grid faults normally done with FRT-containers
- FRT containers designed for high power ratings ($100 \text{ kW} < P < 6 \text{ MVA}$)
- Not applicable for string inverters ($P < 20 \text{ kW}$)
- NS-FRT tests with network simulator
 - Calculation of voltage phasors at LV network for faults (3phase and 2 phase) in HV and MV networks
 - Real reproduction of voltage curves with low ohmic programmable AC-network sources
 - Real emulation of network impedance by adjustable R-L-network



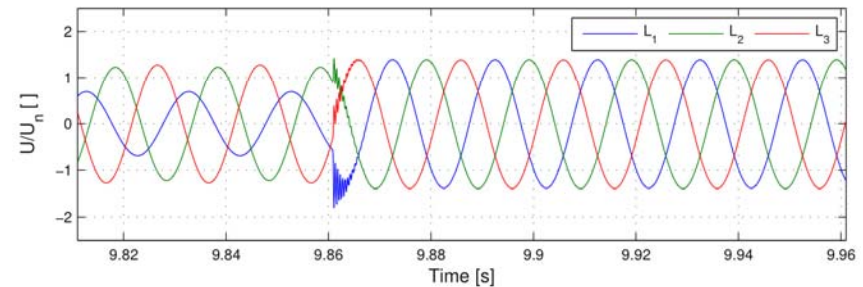
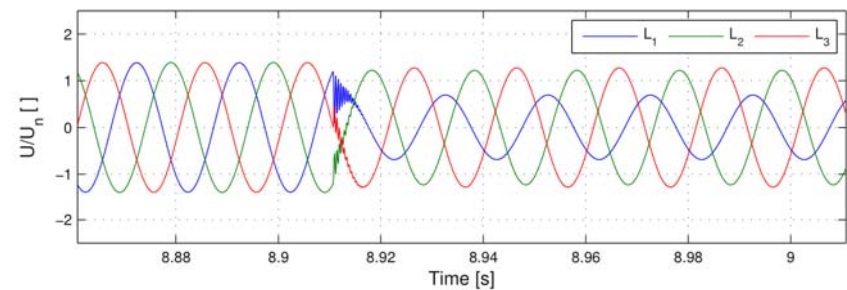
2. Power System Services of PV-systems

Test procedures for PV-systems – Testing procedures

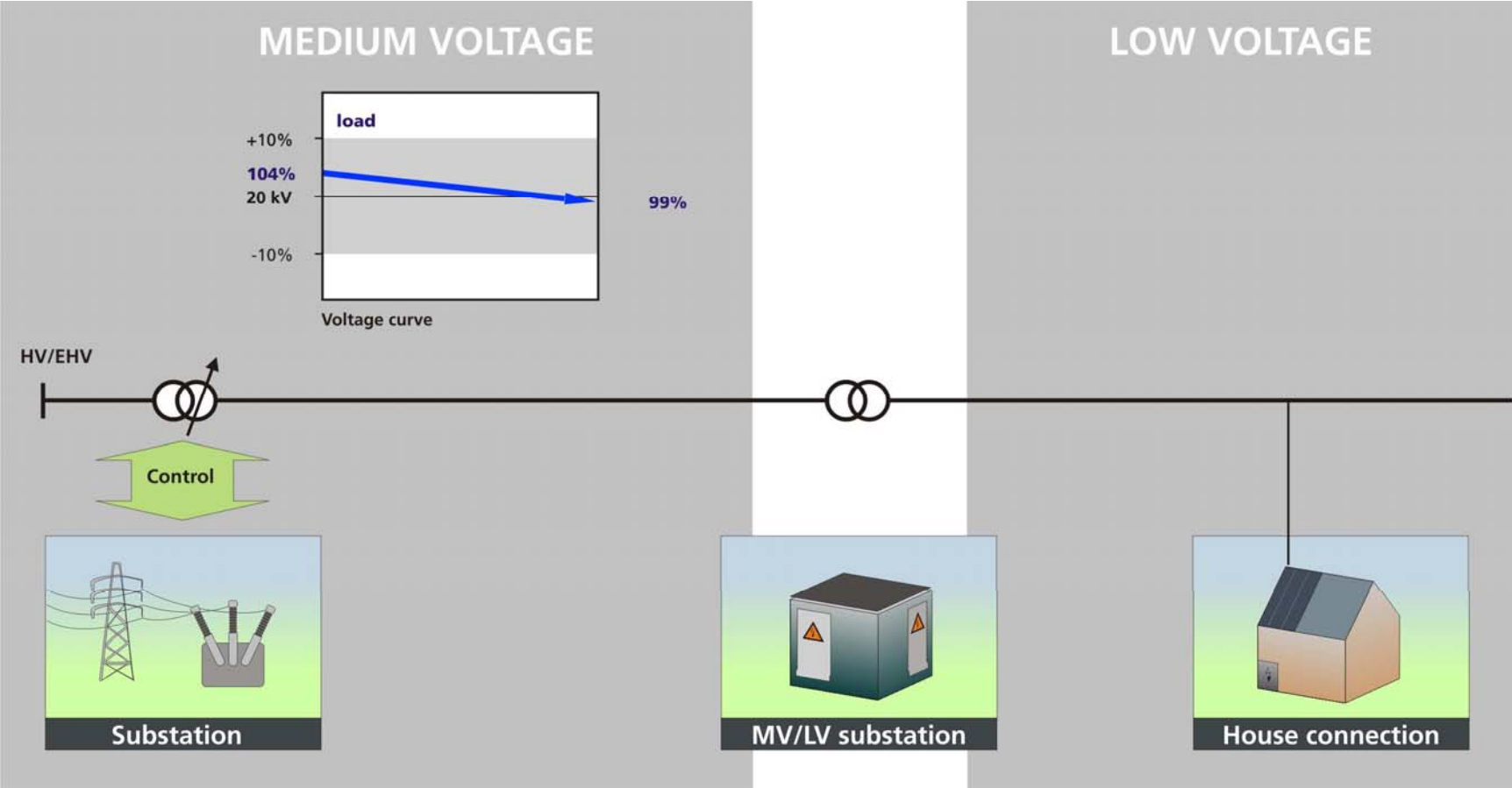
- Unbalanced 2 phase fault
- MV/LV transformer: Dd



- Unbalanced 2 phase fault
- MV/LV transformer: Dy

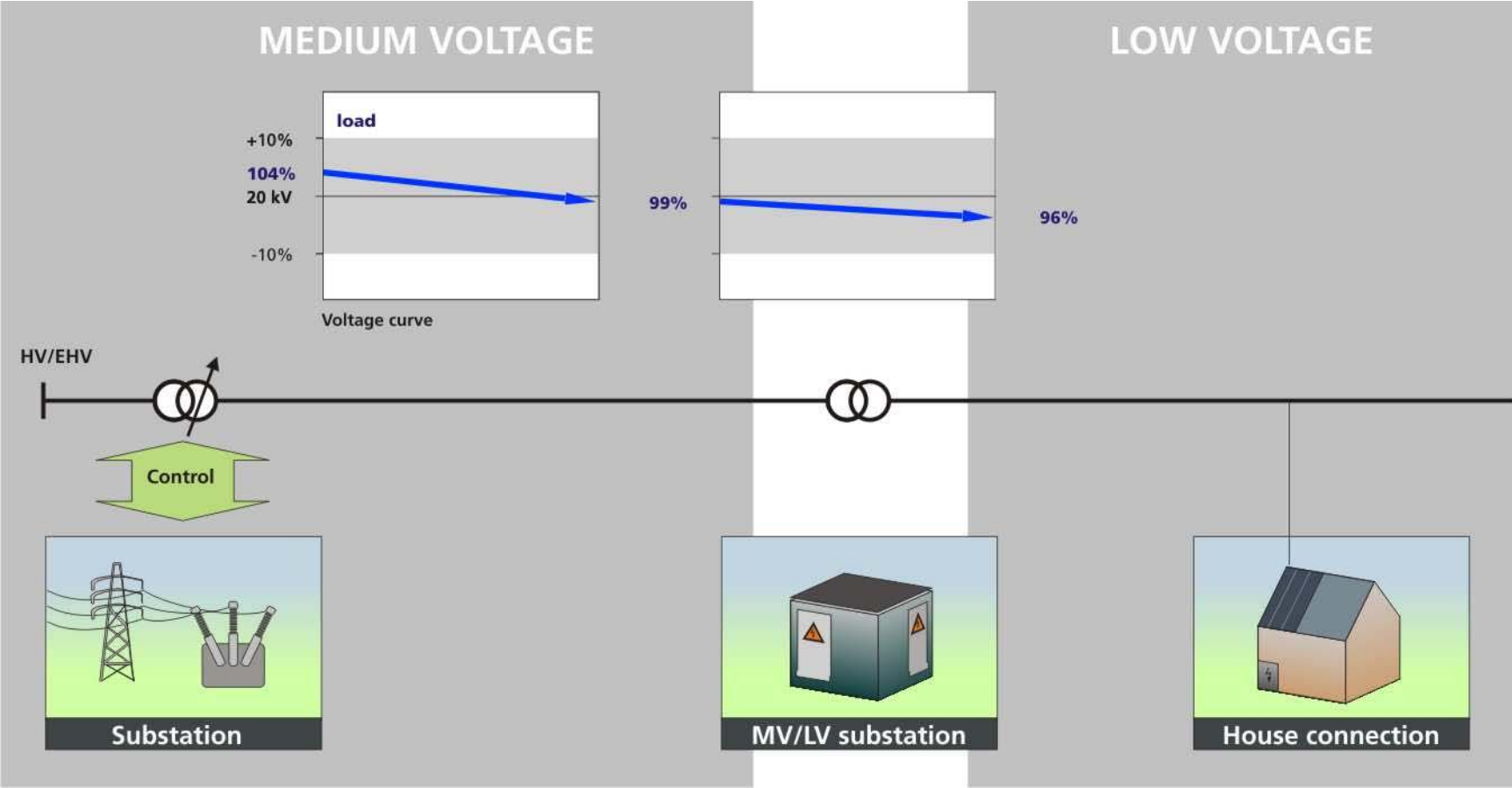


3. Application of power system services Voltage Control

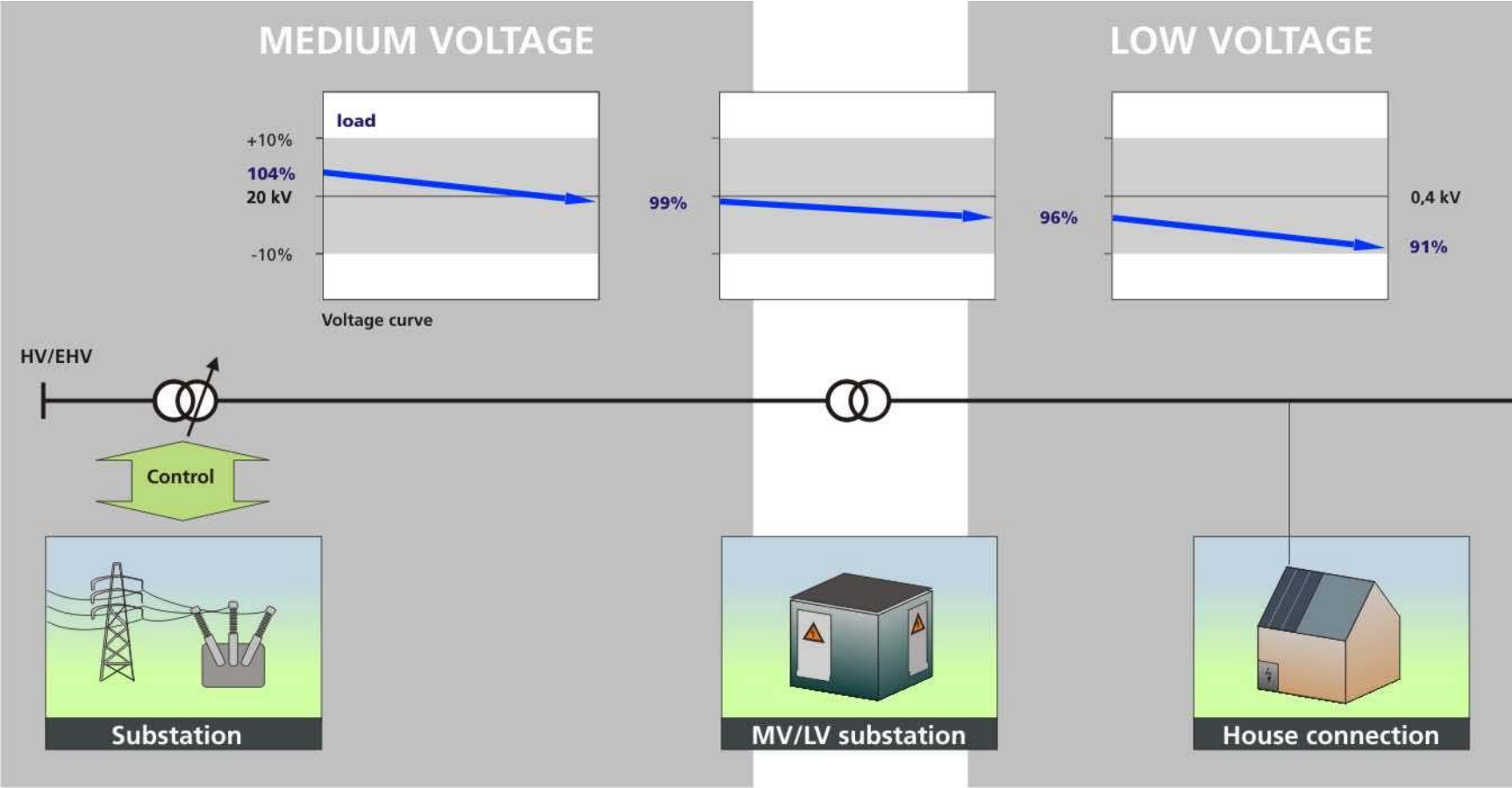


3. Application of power system services

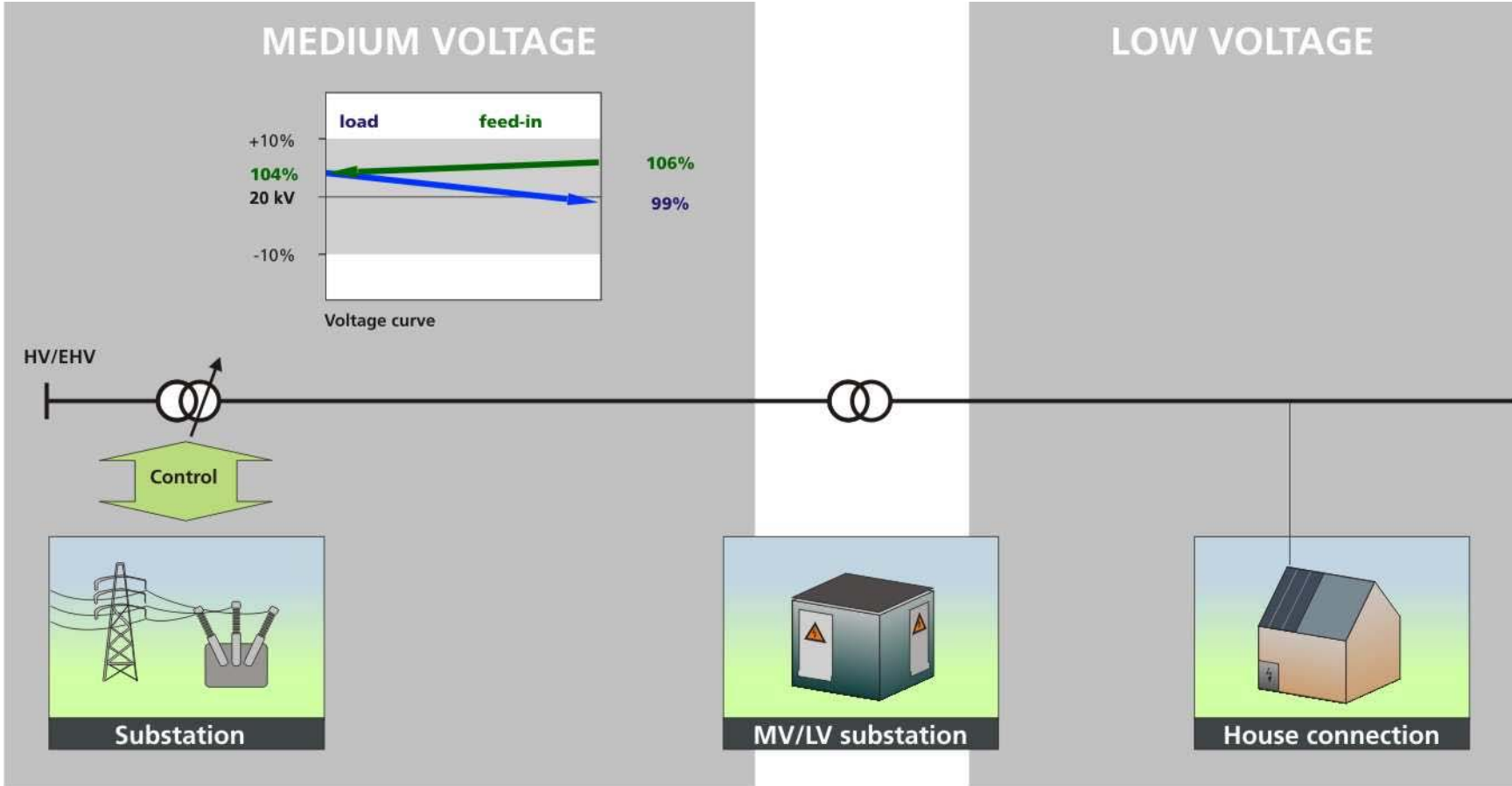
Voltage Control



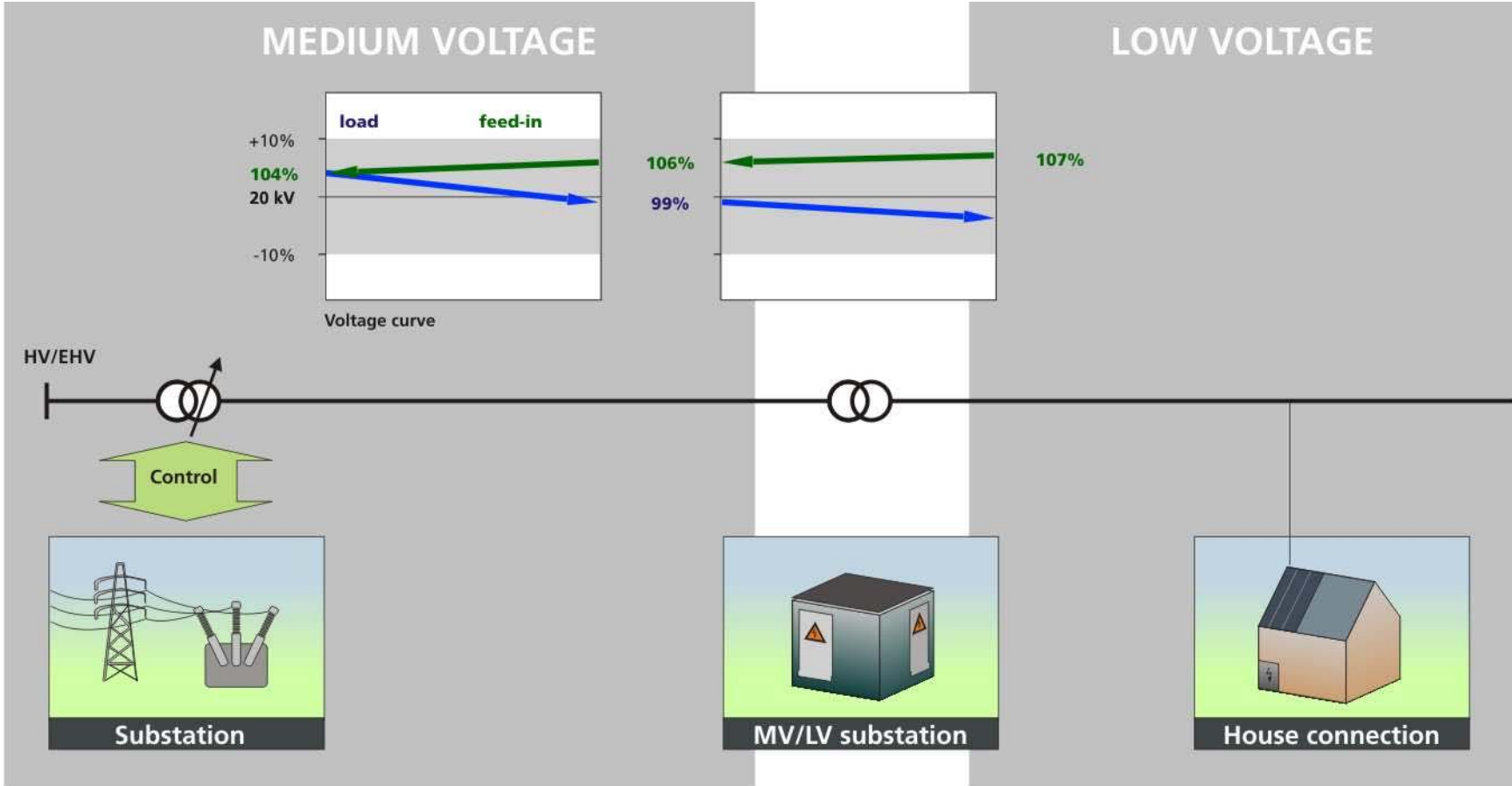
3. Application of power system services Voltage Control



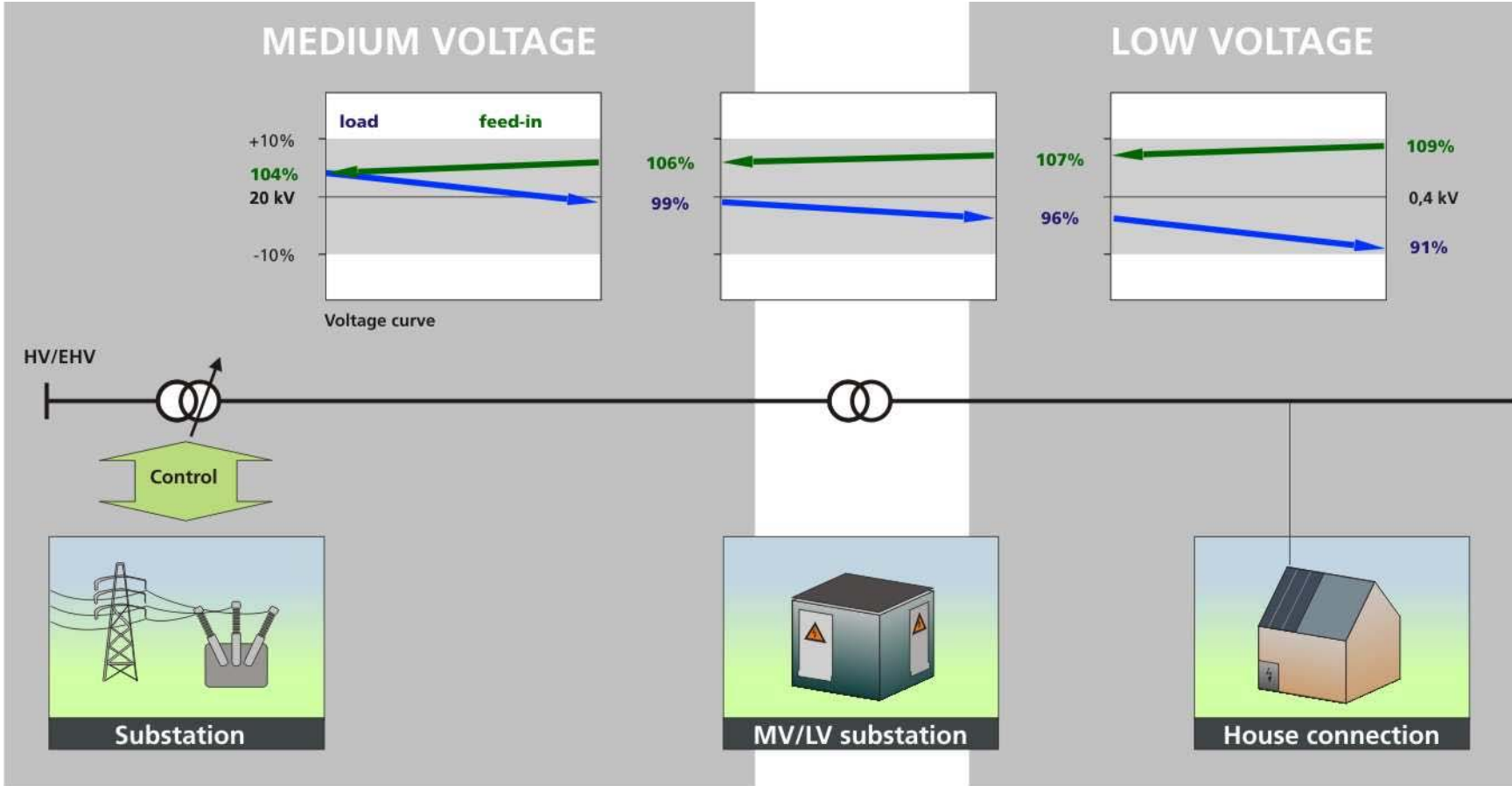
3. Application of power system services Voltage Control



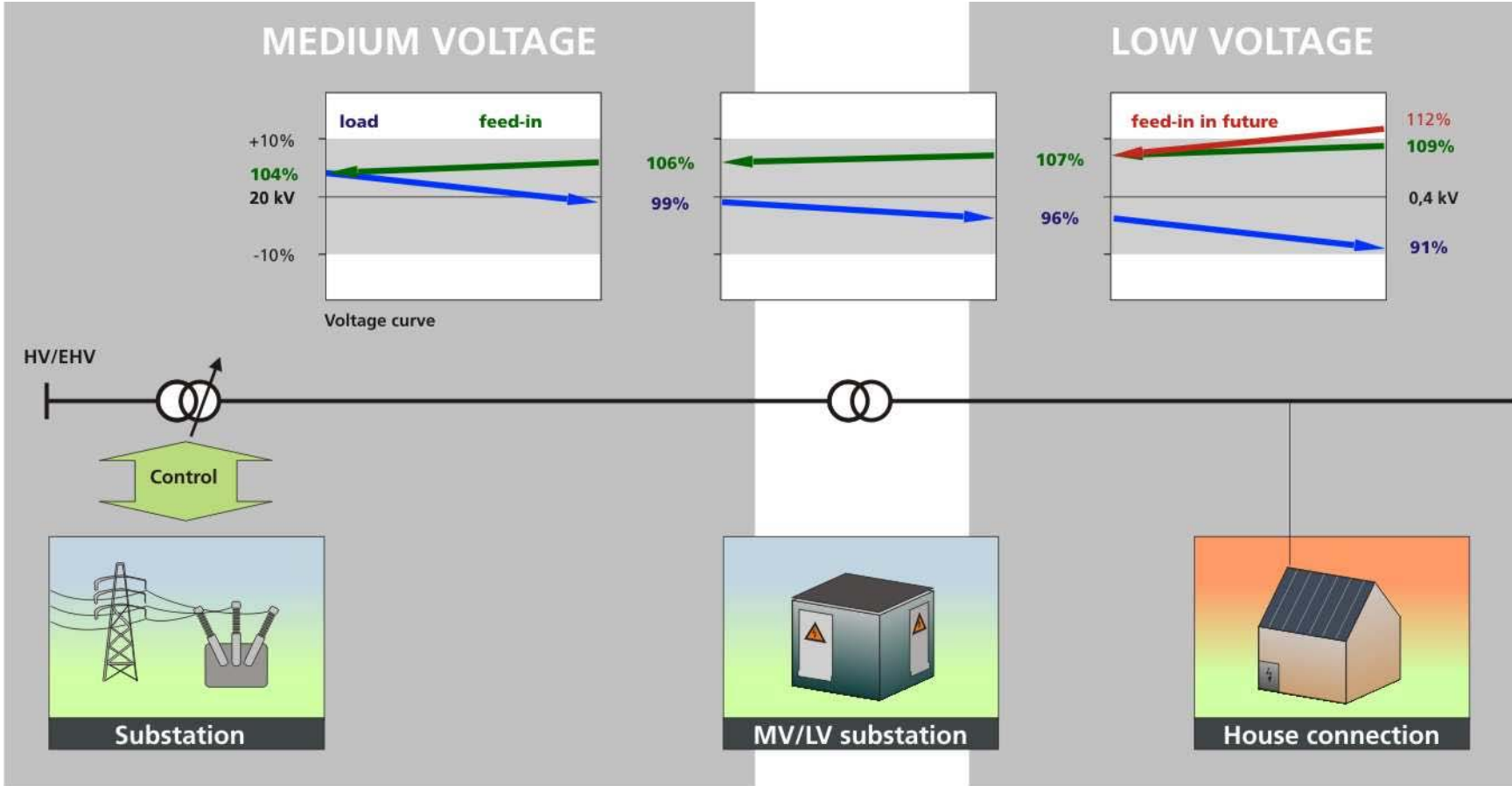
3. Application of power system services Voltage Control



3. Application of power system services Voltage Control



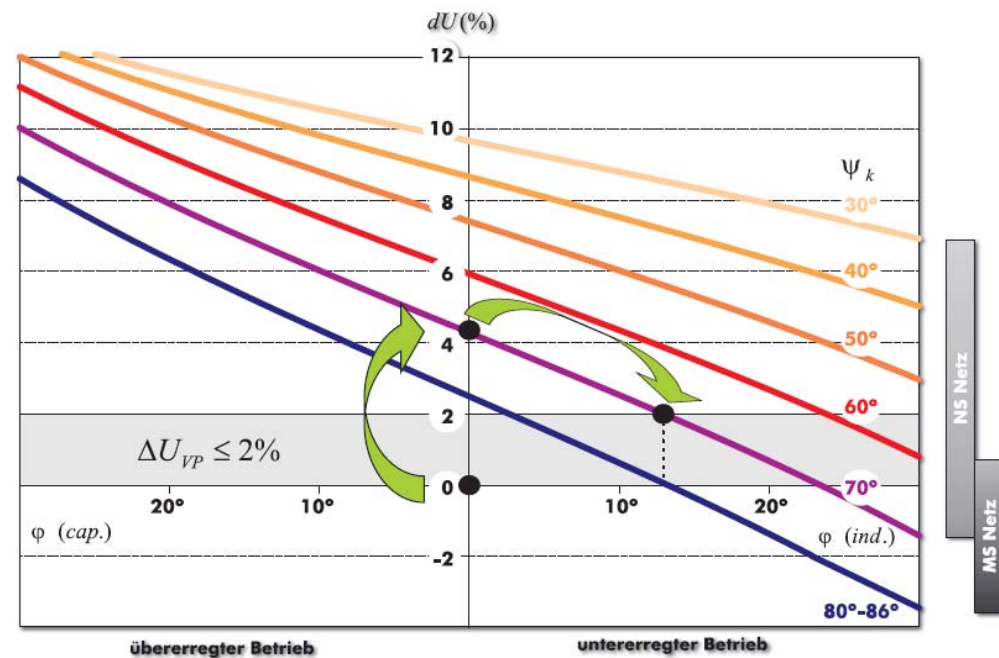
3. Application of power system services Voltage Control



3. Application of power system services Voltage Control – Reactive power

- Selective voltage change by power factor control of DER unit
 - ψ_k : network impedance angle
 - S_{SC} : Short circuit power
 - $S_{A,max}$: nominal power of DER unit

$$\Delta u_{aV} = \frac{S_{A,max} \cdot \cos(\Psi_{kV} + \varphi)}{S_{SC}}$$



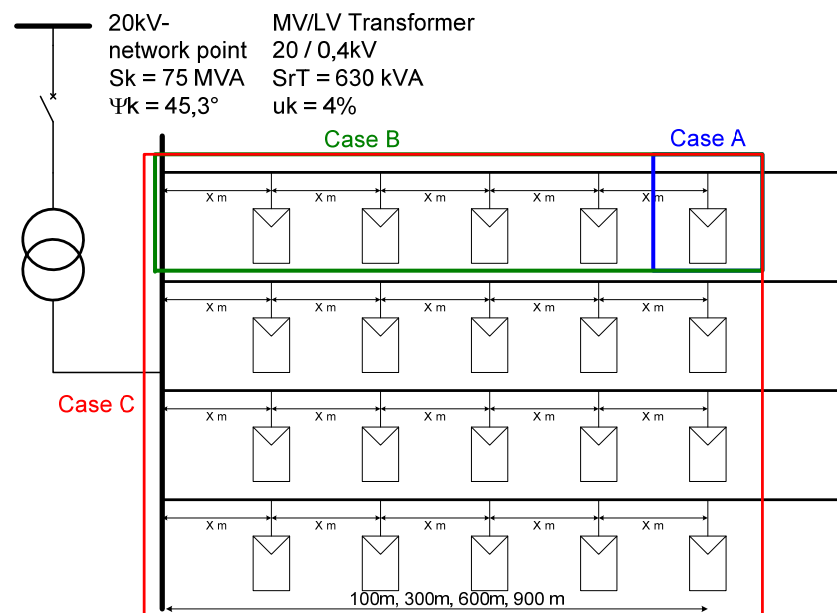
Source: B. Valov, Volle Nutzung der Netzkapazität und Spannungstabilisierung durch neues Auslegungskonzept für PV-Kraftwerke, 24. Symposium Photovoltaische Solarenergie, Bad Staffelstein, 2009

Slide 32, Power System Service Seminar, 31.03.2011

3. Application of power system services

Voltage Control – Case studies

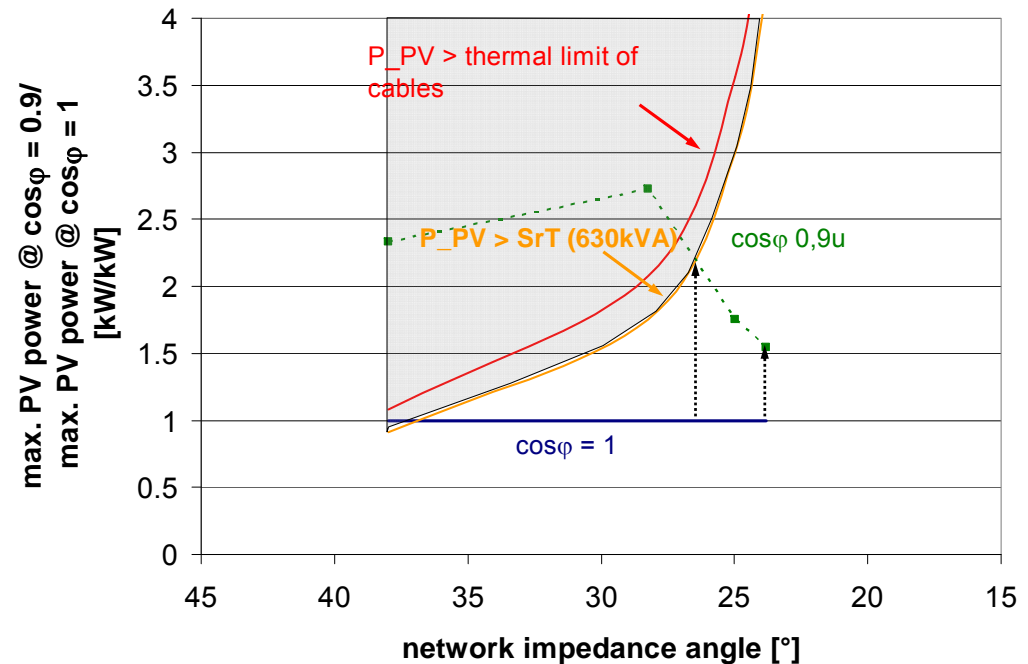
- Generic network case studies
 - Case A: Single feeder network, single PV-system
 - Case B: Single feeder network, five PV-systems
 - Case C: Four feeders, each with 5 PV-systems
 - Different feeders length are considered (100m, 300, 600, 900m)



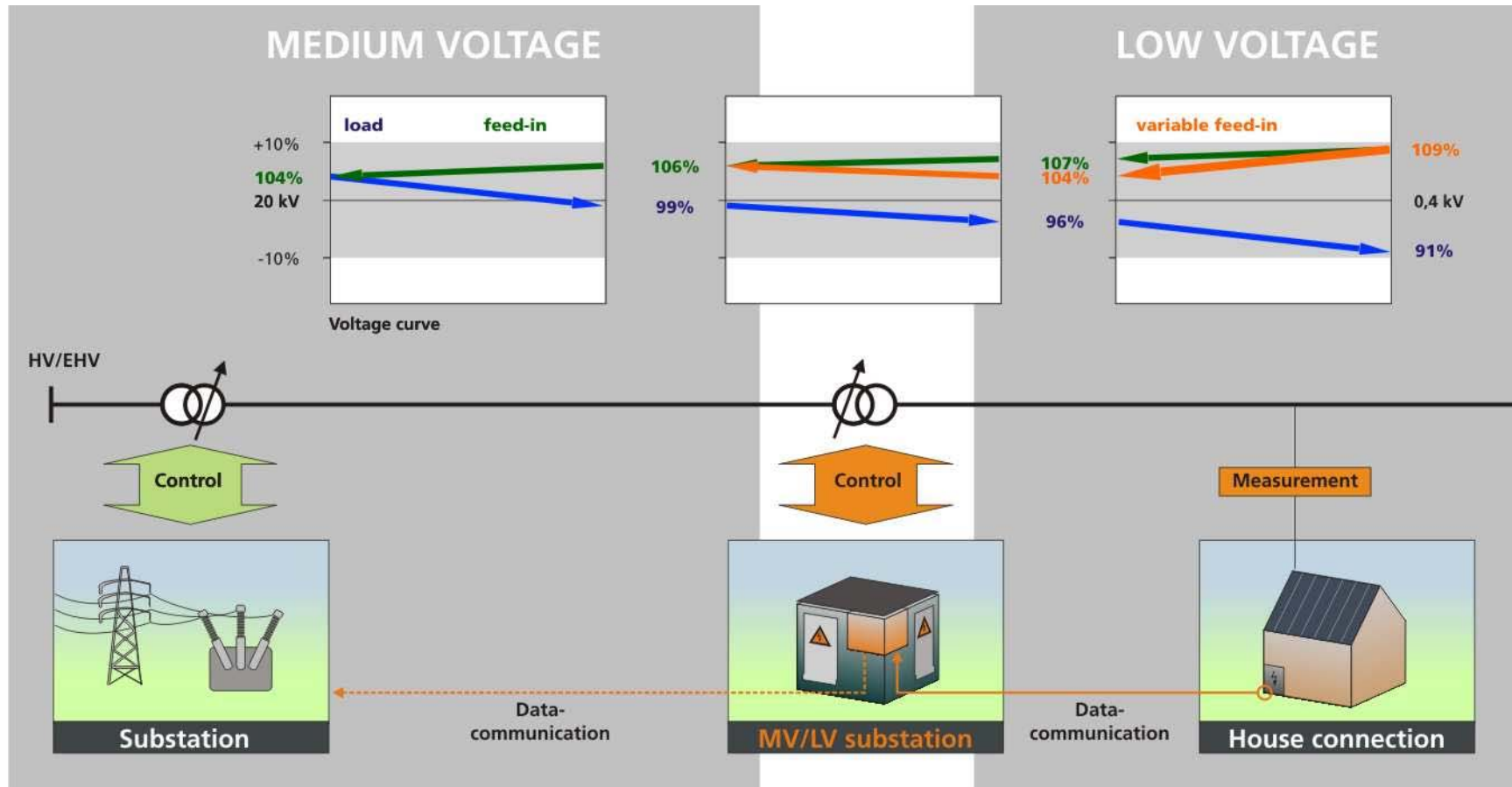
3. Application of power system services

Voltage Control – Potential of reactive power

- Case C: 4 feeder, 5 PV-systems per feeder, $\cos \varphi=0.9$, max. voltage rise 3%
- Relative increase of connectable PV systems due to reactive power voltage control varies between 1.5 and more than 2.
- At larger network impedance angles (resp. short feeder) the thermal limits of the network transformer or the cables may be reached.
- Example ($S_k = 1,2 \text{ MVA}$, $\Psi_k = 25^\circ$, 4x5 PV-systems)
 - $\cos \varphi = 1.0$: 216 kW in total
 - $\cos \varphi = 0.9$: 378 kW in total (factor of 1.75)



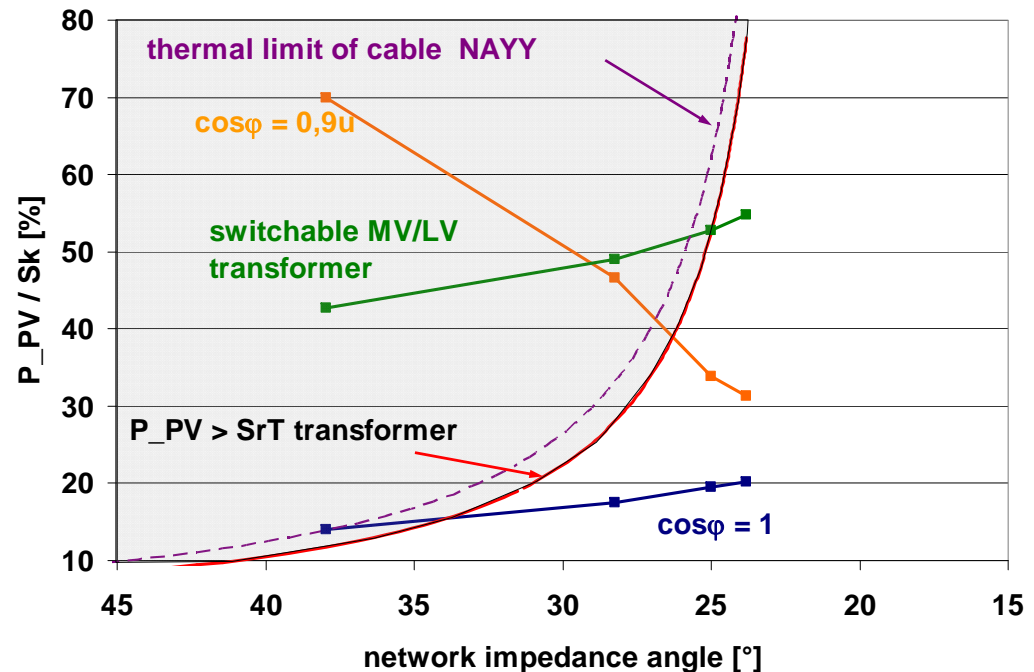
3. Application of power system services Voltage Control – Active network components



3. Application of power system services

Voltage Control – Active network components

- Extended Use of the available voltage band
 - Case C: 4 feeder, 5 PV-systems per feeder
- Switchable MV/LV transformers provide an alternative way to control the voltage in LV networks.
 - transformer with steps $2x \pm 2.5\%$
 - allowed voltage rise increases from 3% to 8%
 - max. connection power increase by a factor of 2.7
- In particular useful for longer feeders
- Example ($S_k = 1,2 \text{ MVA}$, $\Psi_k = 25^\circ$, 4x5 PV-systems)
 - $\cos \varphi = 1.0$: 216 kW in total
 - $\cos \varphi = 0.9$: 378 kW in total
 - Smart transformer: 538 kW in total



4. Conclusions

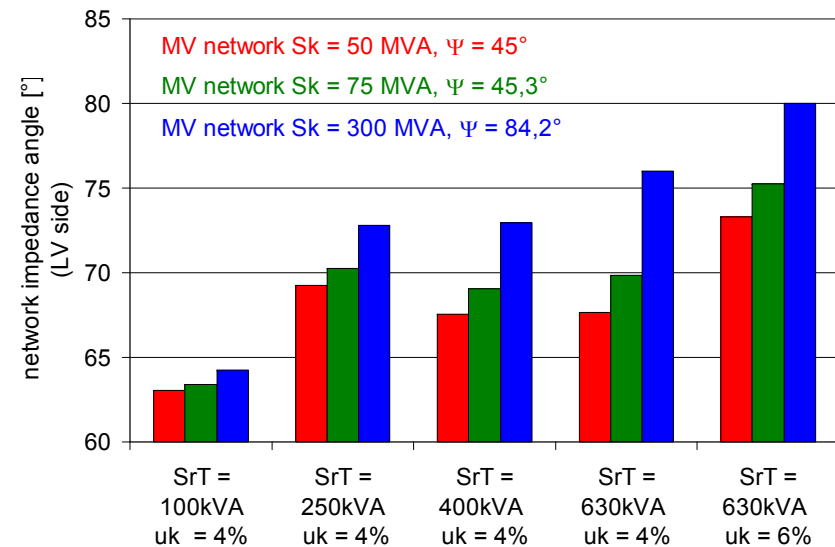
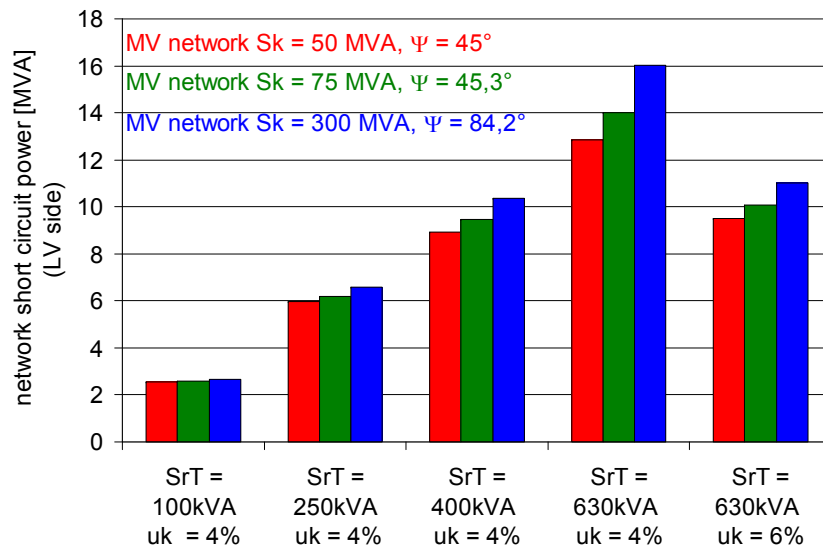
- Share of renewable energy sources increases
- Power system services
 - are required to keep network stability
 - are required to overcome network constraints for further increase of renewable generation
- PV-systems are well suited to provide power system services
 - Grid Codes describe technical requirements for DER units
 - Intensive testing of conformity with guideline is required
- Application of power system services of PV-systems
 - Voltage control is a major objective in distribution networks
 - By using reactive power voltage control the maximum permissible PV power may be increased by a factor 1.5 up to more than 2 (for the analyzed generic networks)
 - Controllable MV/LV transformer allows to connect 2.7 more PV power to the network compared to the normal case (suited for long feeders)

Backup

3. Application of power system services

Voltage Control – Effect of network parameters

- S_k and Ψ_k at the LV bus-bar of the MV/LV substation
 - Short circuit power and network impedance angle at the LV bus-bar of the MV/LV substation are mainly determined by the transformer
 - In particular the short circuit power (S_k) can be well estimated from apparent power (S_{rT}) and short circuit voltage (u_k) of the MV/LV transformer.

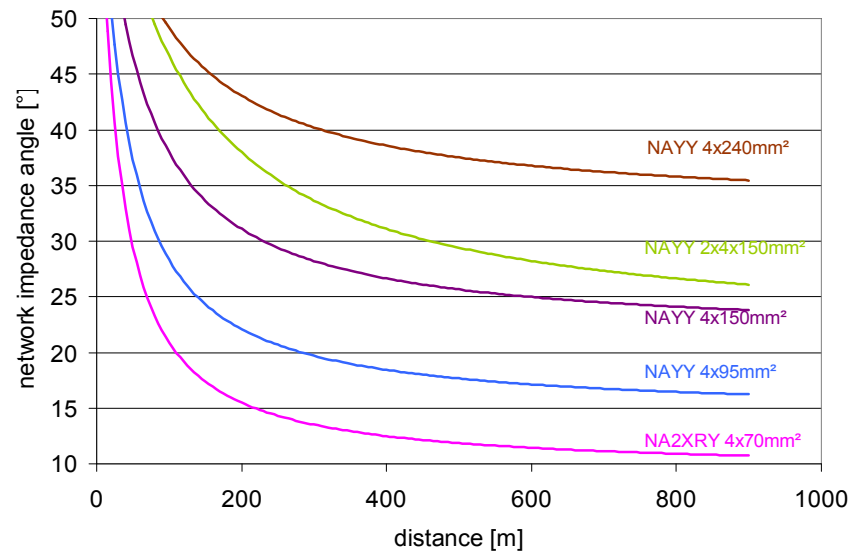
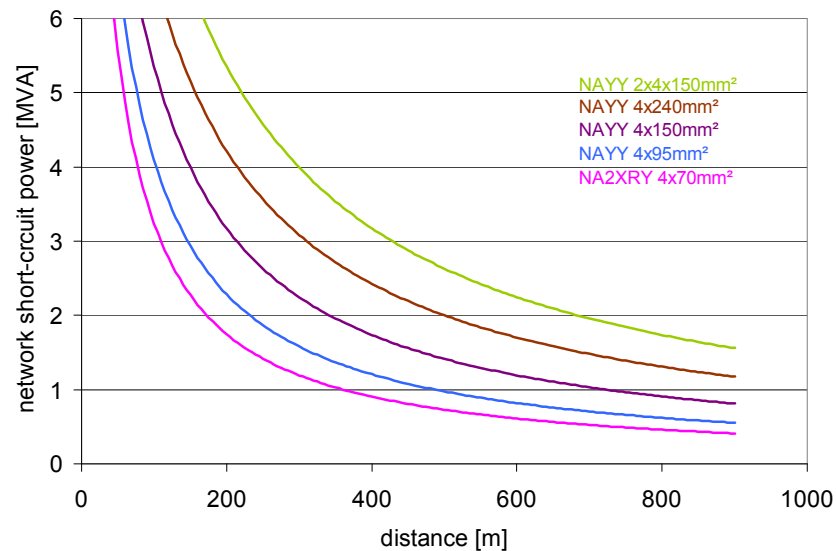


3. Application of power system services

Voltage Control – Effect of network parameters

■ Effect of different cable types

- S_k and Ψ_k decrease with increasing distance to the substation
- The cable type determines how fast S_k and Ψ_k decrease
- At long distances the effect of the cable type dominates
- Example: 600m distance, NAYY 4x150mm² → $S_k = 1,2$ MVA; $\Psi_k = 25^\circ$



3. Application of power system services

Voltage Control – Maximum permissible connection power

- Power factor $\cos \varphi=1$, max. voltage rise 3%)
 - S_k and Ψ_k at the end of the feeder are sufficient to describe maximum permissible PV power
 - The serial placement of PV systems leads to a higher amount of connectable power because of the lower voltage rise of the PV systems connected to stronger network points
 - Case C (parallel feeders) results in similar curves, but per feeder PV power is lower, because of the voltage rise in the substations LV-busbar

