
IMPROVING AND MONITORING THE MAGNETIC PULSE WELDING PROCESS BETWEEN DISSIMILAR METALS

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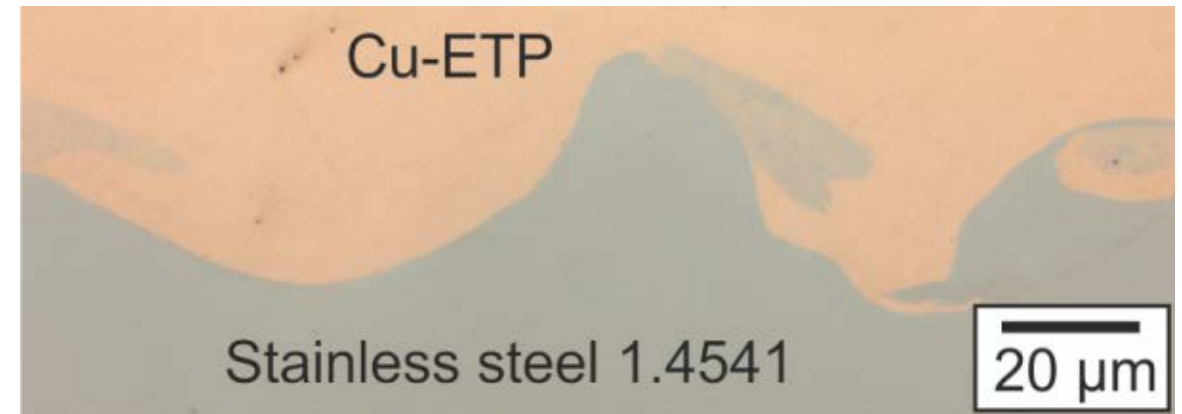
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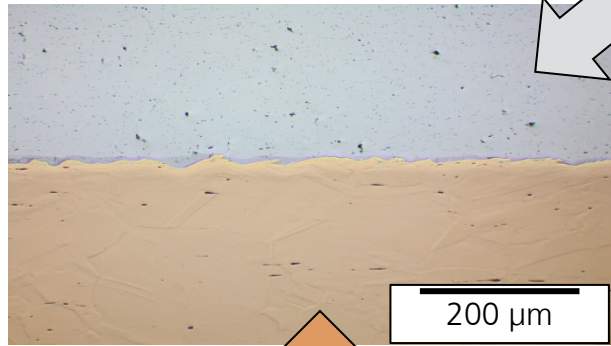
AGENDA

- Taking advantage of magnetic pulse welding (MPW)
- Facing the challenges of MPW
- Characterizing the high-speed impact
- Reducing the impact energy during MPW
- Testing of magnetic pulse welded joints
- Concluding remarks
- Competences at IWS

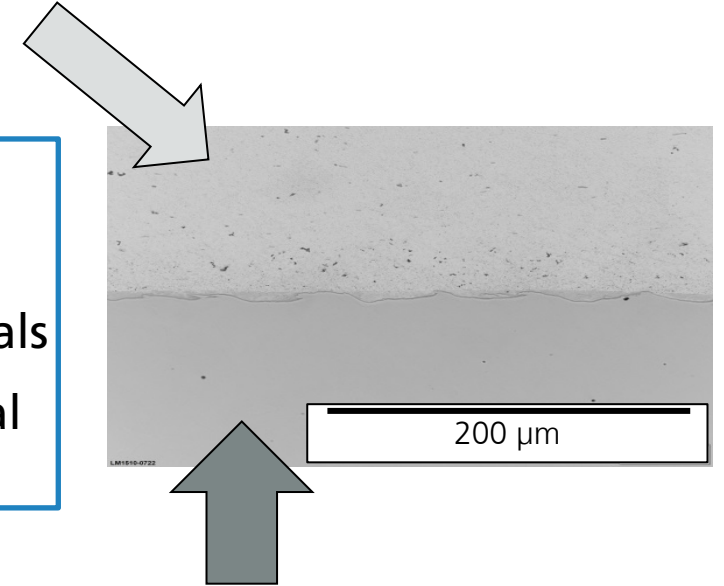


Advantages of MPW Dissimilar metal welding

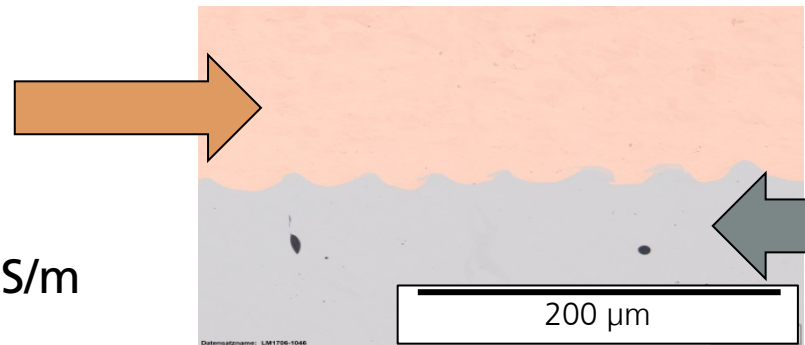
Aluminum
Melting point $\approx 660^\circ\text{C}$
Density $\approx 2.7\text{ g/cm}^3$
Electrical conductivity $\approx 37\text{ MS/m}$



Exemplary motivations:
Realizing lightweight design
Substituting expensive or rare materials
Combining distinct different material properties within one part



Copper
Melting point $\approx 1085^\circ\text{C}$
Density $\approx 8.9\text{ g/cm}^3$
Electrical conductivity $\approx 58\text{ MS/m}$



Steel (S235)
Melting point $\approx 1250\text{-}1460^\circ\text{C}$
Density $\approx 7.8\text{ g/cm}^3$
Electrical conductivity $\approx 10\text{ MS/m}$

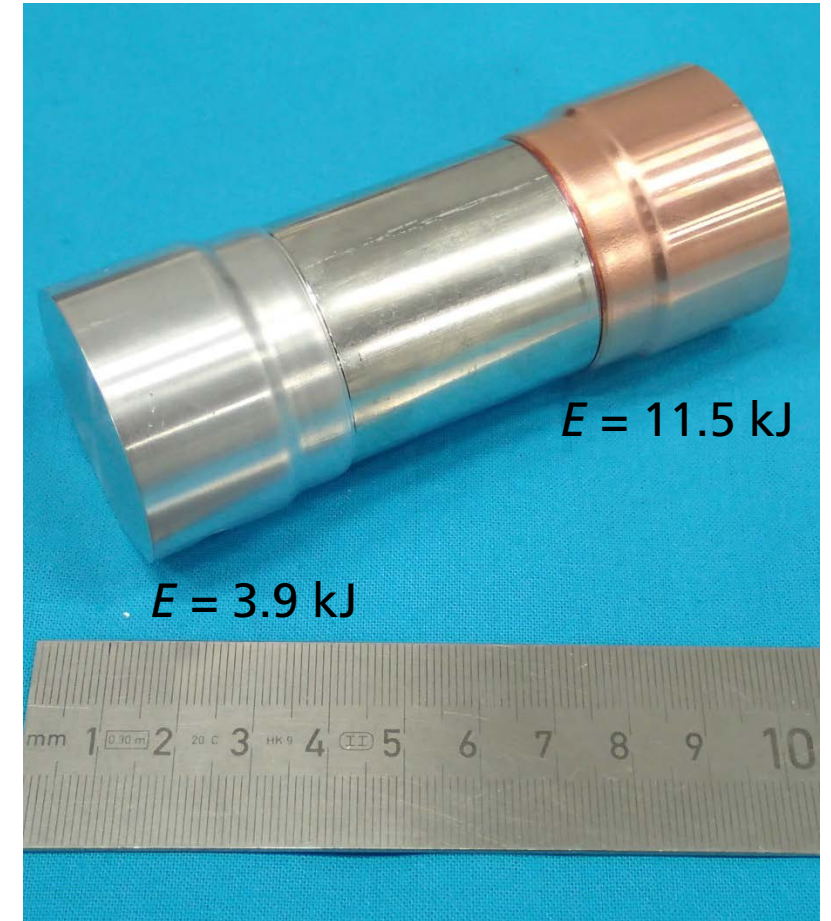
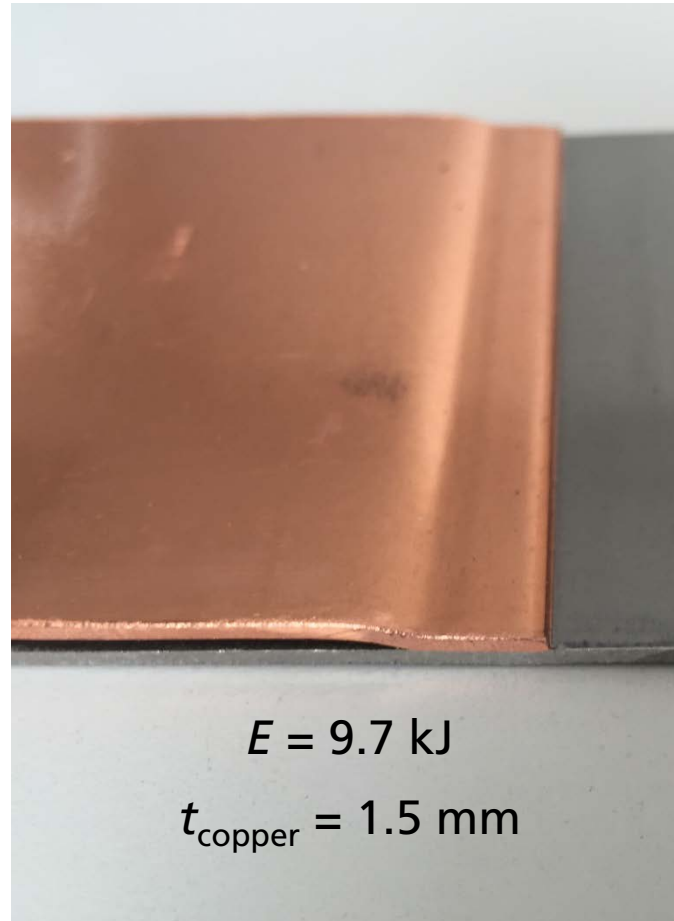
Advantages of MPW

Possible joining configurations

Examples

Welding geometries

- Sheet-to-sheet or sheet-to-profile welding with flat coils
- Tube-to-tube or tube-to-cylinder welding with one turn coils or multi-turn coils with fieldshapers (compression or expansion)



Advantages of MPW

Applications for tubular welding

Case studies

Material combinations

Hybrid drive shaft (left)

- Steel and aluminum

Multi-material part (right)

- Aluminum and stainless steel
- Copper and stainless steel

C45 (1.0503)
 $t = 11.5 \text{ mm}$

EN AW-6060 T66
 $t = 2 \text{ mm}$

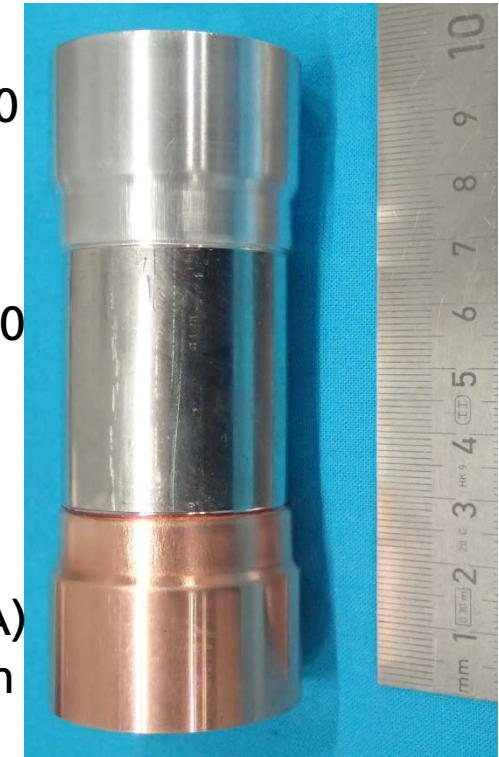


Drive shaft:
torque transmission

EN AW-1050
 $t = 1 \text{ mm}$

X6CrNiTi18-10
(1.4541)
 $t = 2 \text{ mm}$

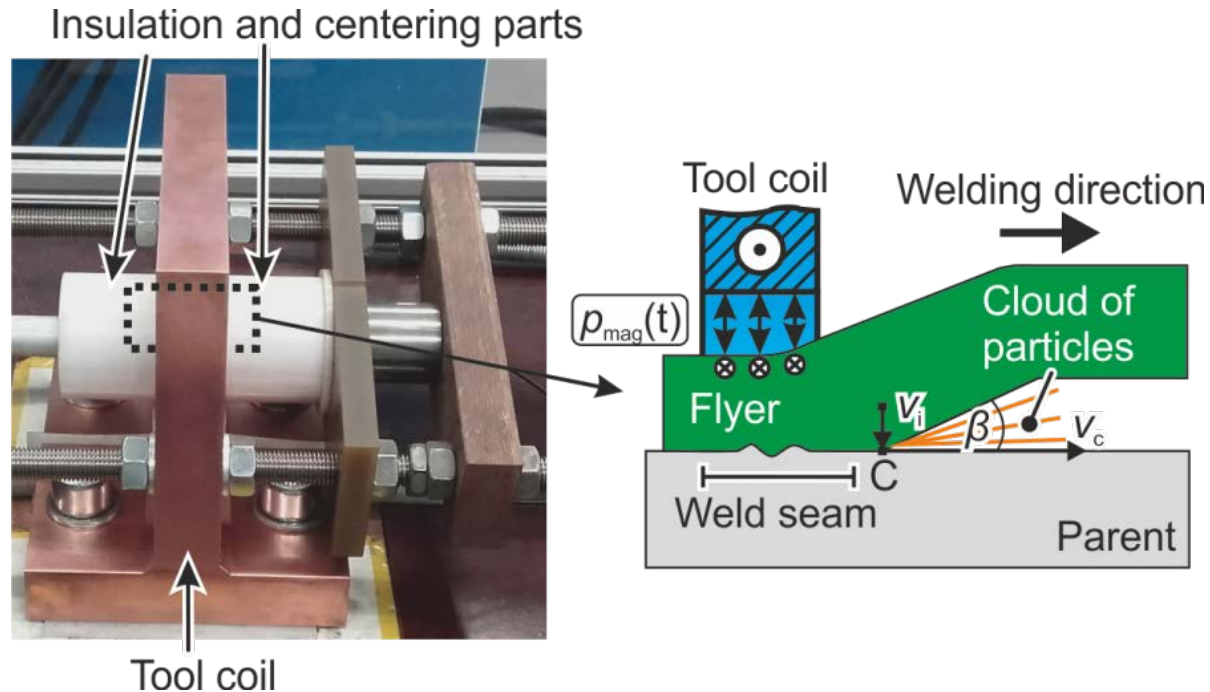
Cu-ETP
(CW004A)
 $t = 1 \text{ mm}$



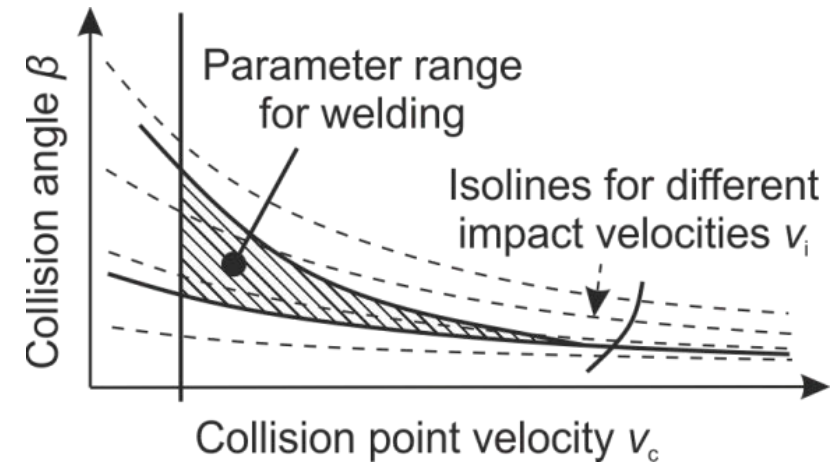
Multi-material part:
thermal isolation and tightness
at low temperatures

Challenges of MPW

Physical background



Schematic of a welding window



- Collision kinetics and welding results depend on multiple factors (geometrical, material and machine related)
- Welding at the lower boundary is aspired to increase the lifetime of the tool coils, but difficult to achieve and to monitor with conventional measurement techniques

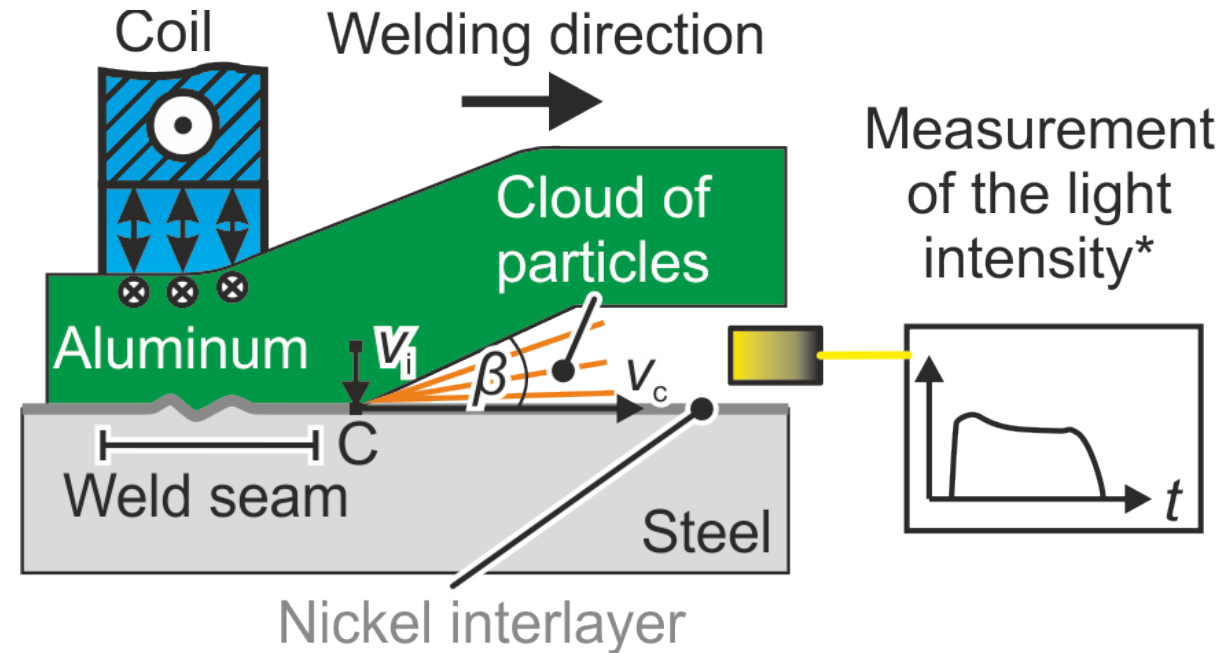
Challenges of MPW

Strategies for process monitoring and improvement

Solutions

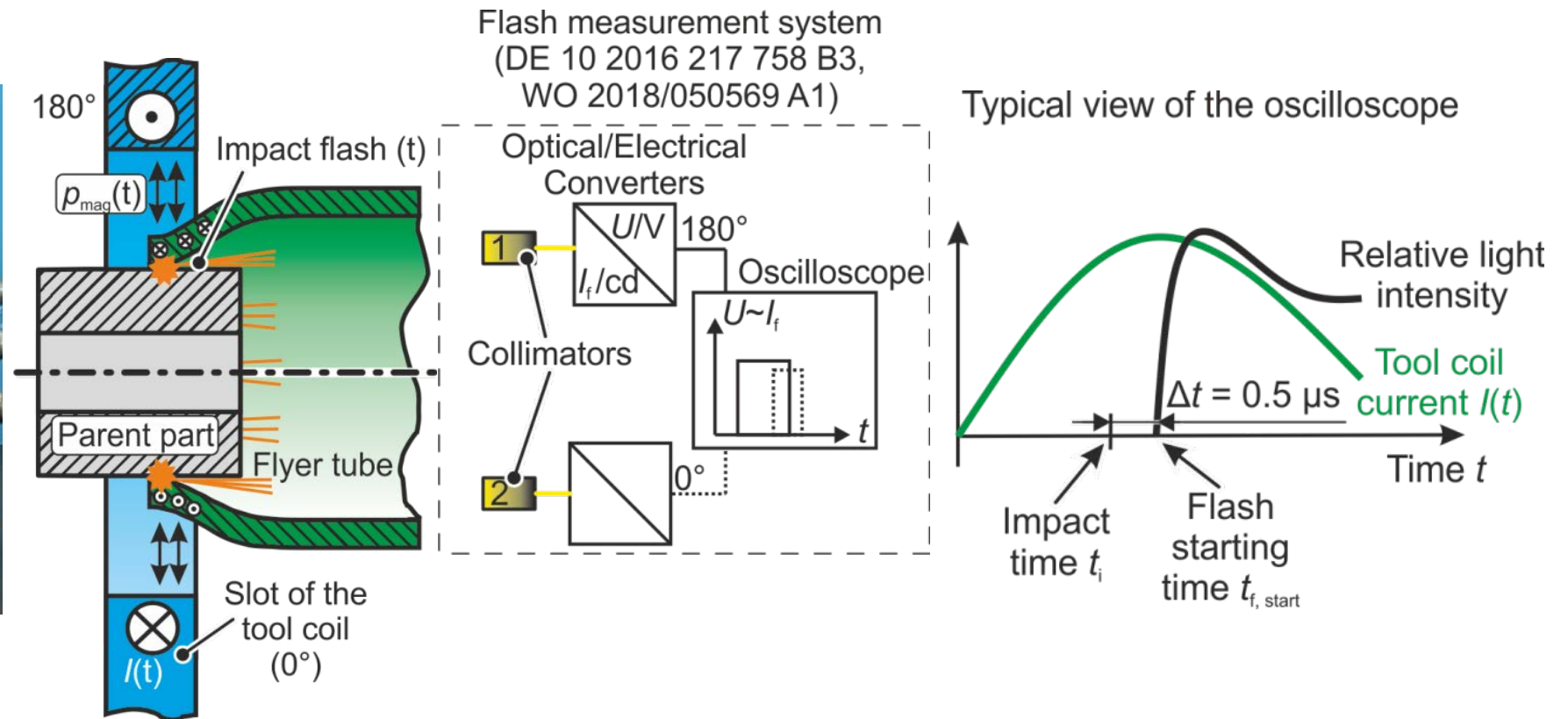
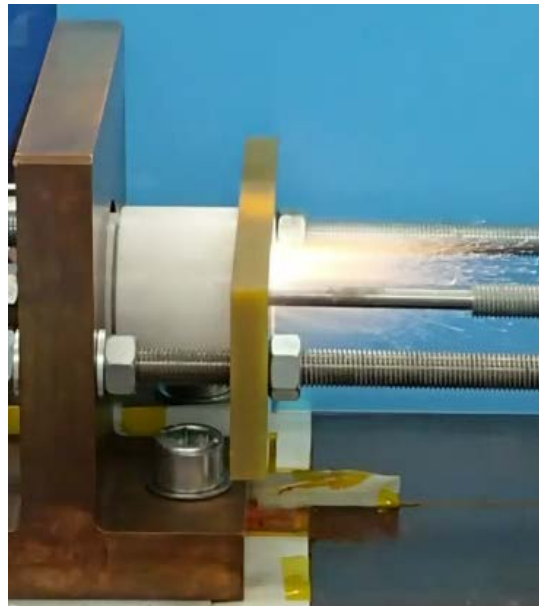
Measurement & Improvement

- Characteristic light emission enables determination of v_i , v_c & β
- Light intensity serves as a necessary welding criterion
- Interlayer of nickel is applied prior MPW on the steel parent



*DE 10 2016 217 758 B3, WO 2018/050569 A1

Characterization of the high-speed impact Flash measurement system



- Reproducible delay of the flash starting time enables the calculation of the impact time t_i
- Impact velocity v_i , axial collision point velocity v_c and collision angle β can be estimated

Characterization of the high-speed impact

Application of the flash measurement system



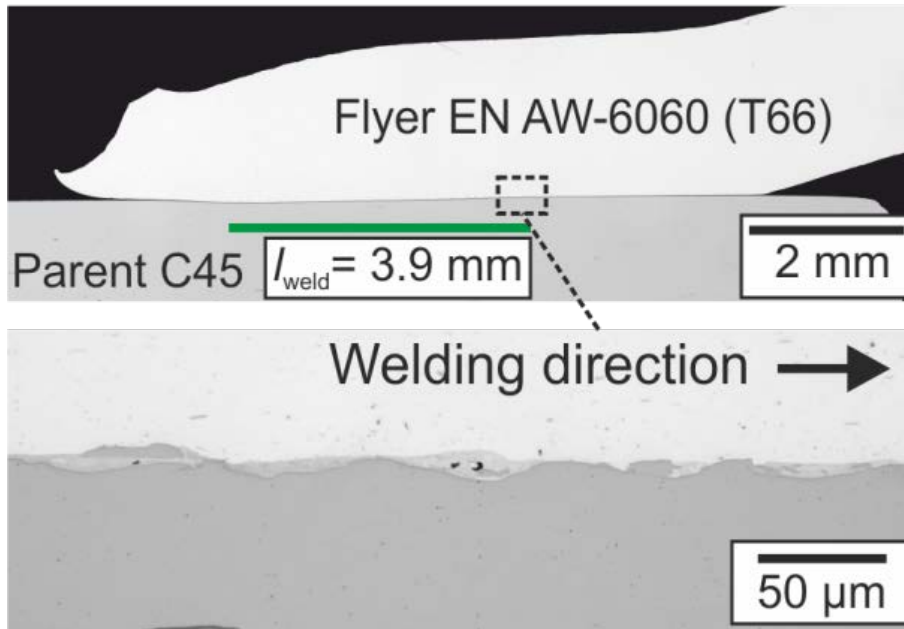
Material combination	Charging energy E	Maximum tool coil current $I(t)$	Starting time of the flash $t_{f,start}$	Calculated radial impact velocity $v_{i,r}$	Circumferential weld
	kJ	kA	μ s	m/s	
Aluminum - steel	2.0	251	19.0	108	Yes
	2.9 ↓	312 ↓	17.2 ↑	120 ↓	Yes
	3.9	360	14.9	139	Yes
Copper - steel	8.0 ↓	504 ↓	14.6 ↑	142 ↓	No
	11.5 ↓	630 ↓	9.3 ↑	227 ↓	Yes

- Measurement system enables the identification of the lowest possible impact velocity for weld formation (welding window)
- Influence of machine and part related parameters on the forming behavior can be studied

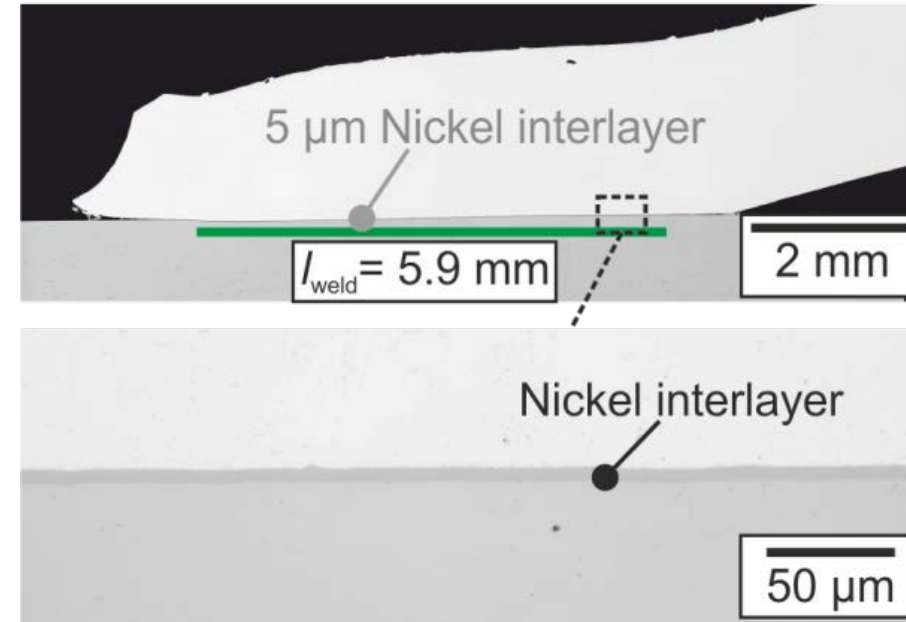
Energy reduction during MPW Influence of reactive interlayers



$E = 8.0 \text{ kJ}$, $I_{\text{max}} = 510 \text{ kA}$, $v_{i,r} = 379 \text{ m/s}$



$E = 5.8 \text{ kJ}$, $I_{\text{max}} = 420 \text{ kA}$, $v_{i,r} = 323 \text{ m/s}$

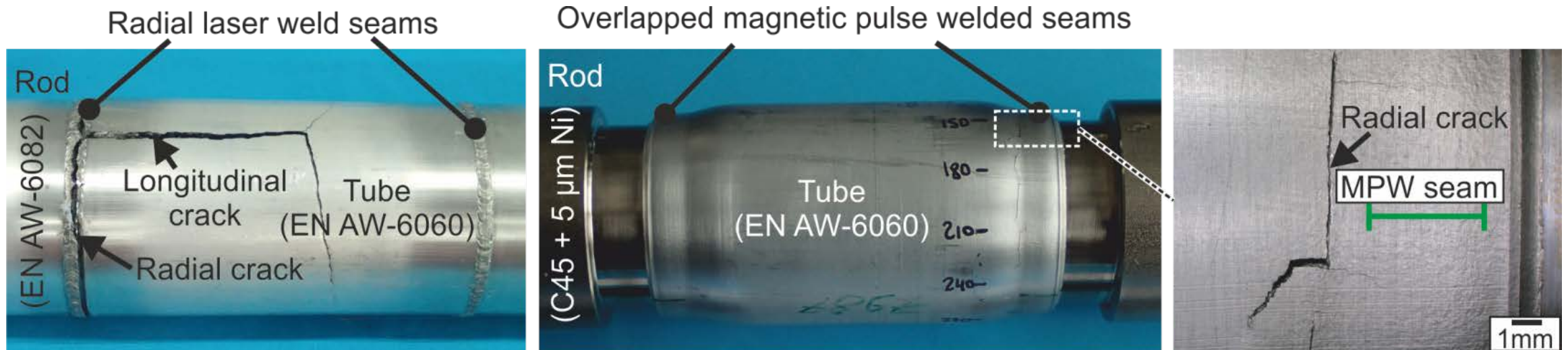


- Nickel interlayer on steel surface enables an energy reduction and extension of the weld seams
- Underlying mechanism is the reaction enthalpy of Al-Ni, which is higher compared to Al-Fe

Testing of MPW parts with nickel interlayer Comparison with laser welded specimens (LBW) under torsional loading



- Same dimensions of the middle section: $\text{Ø}40 \times 2 \text{ mm}$ EN AW-6060 T66
- Increase of the overall static load bearing capability from 558 Nm (LBW) to 737 Nm (MPW)
- Slight increase of the alternating torsional load for a failure probability of 50 % from 113 Nm (LBW) to 127 Nm (MPW)

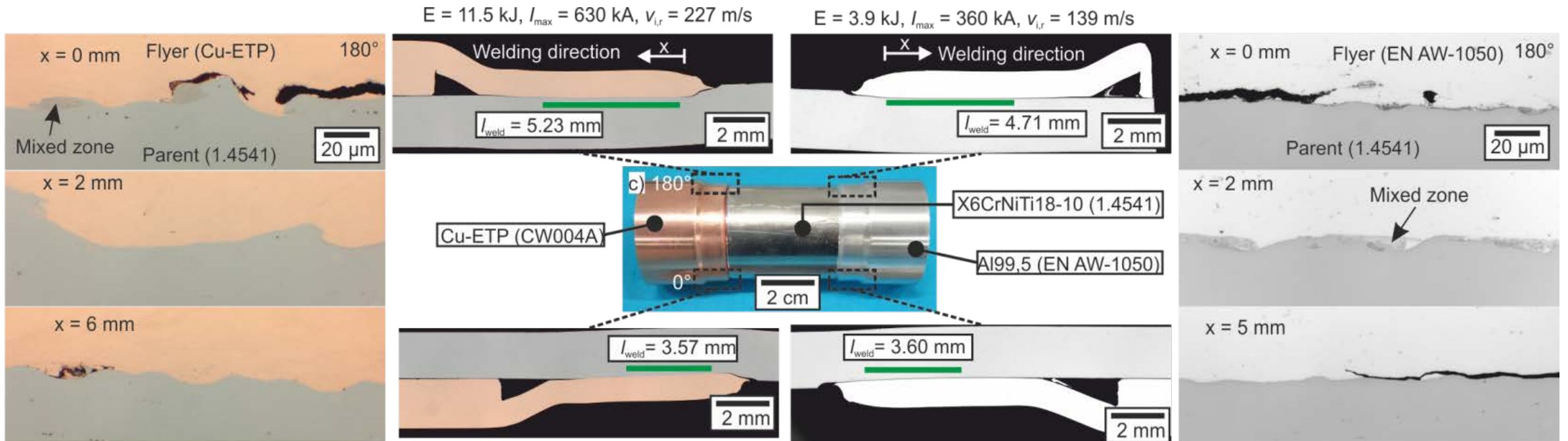


Testing of MPW parts

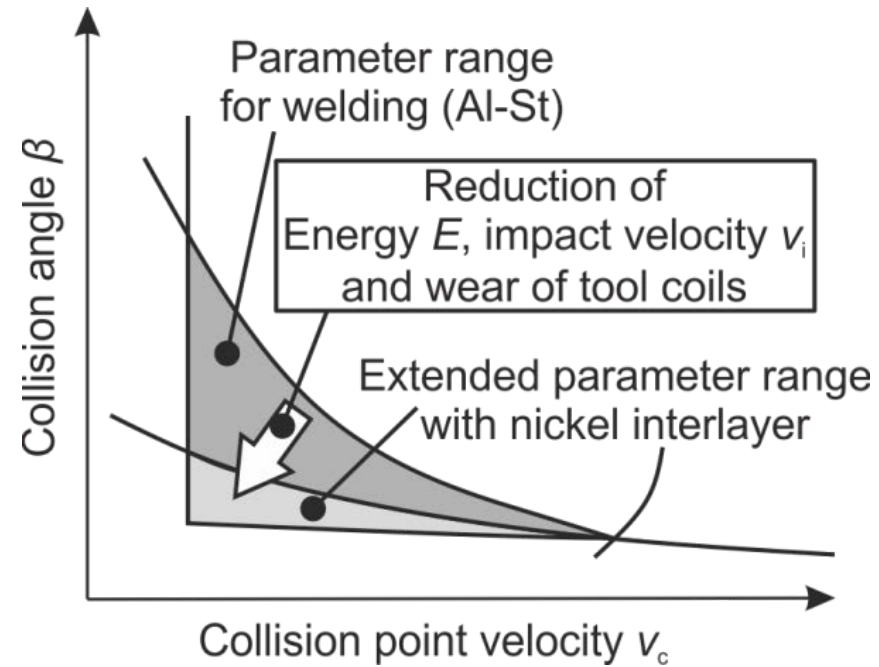
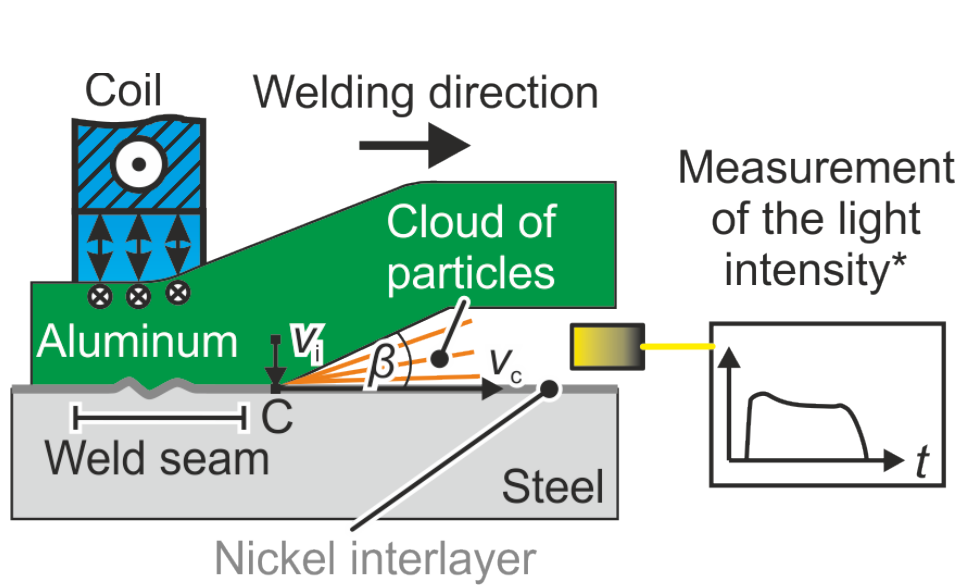
Leakage testing and metallographic analysis



- 15 times: shock cooling and heating from room temperature to 77 K and vice versa
- Proof of leak-tightness with an inner pressure of 10^{-2} mbar at both temperature levels



Conclusions



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Highlights

- New optical measurement system
- Improved MPW process with nickel interlayers
- Reduced energy input during MPW
- High mechanical strength



Competences at Fraunhofer IWS

Magnetic Pulse Welding

Our service

- Consulting and feasibility studies
- Research & development in cooperation with partners from industry and also within public projects
- Tool and system development
- Industrialization



Contact and Acknowledgment

<Video>



Thank you for your attention!

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