



# Influence of Selected Coatings on the Welding Result During Magnetic Pulse Welding (MPW)

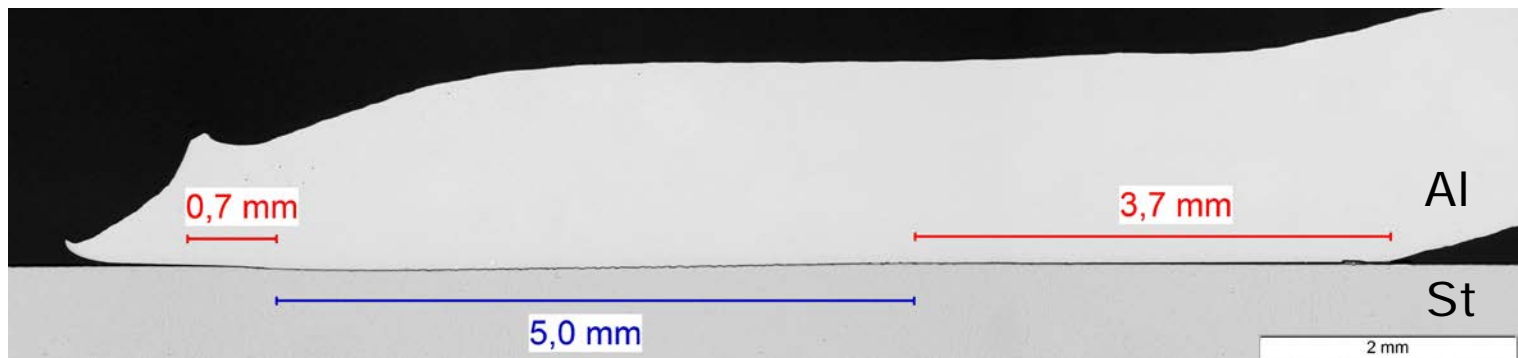
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Dresden, 24.02.2016

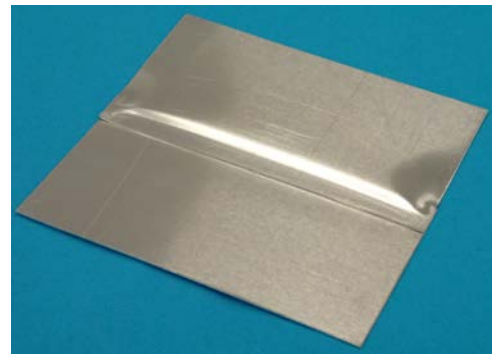
## Agenda

1. Motivation for MPW
2. Experiments with coatings and results
3. Classification of coatings
4. Tailored joining: Outlook

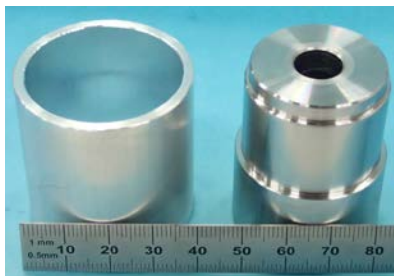
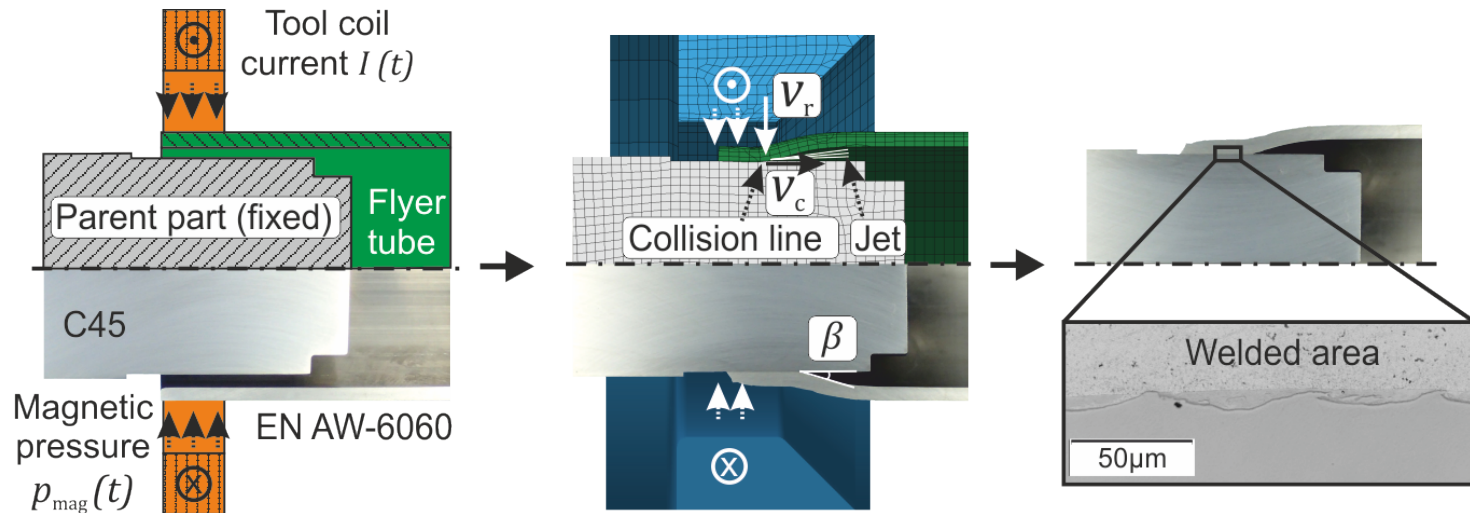


## 1. Motivation for MPW

- **Outstanding:** Similar and dissimilar metal joining
- **Wide ranging:** Applicable for tubular and flat parts
- **Nice side effects:** Fast and clean
- **Surface preparation:**
  - Mechanical treating
  - Cleaning
  - Coating



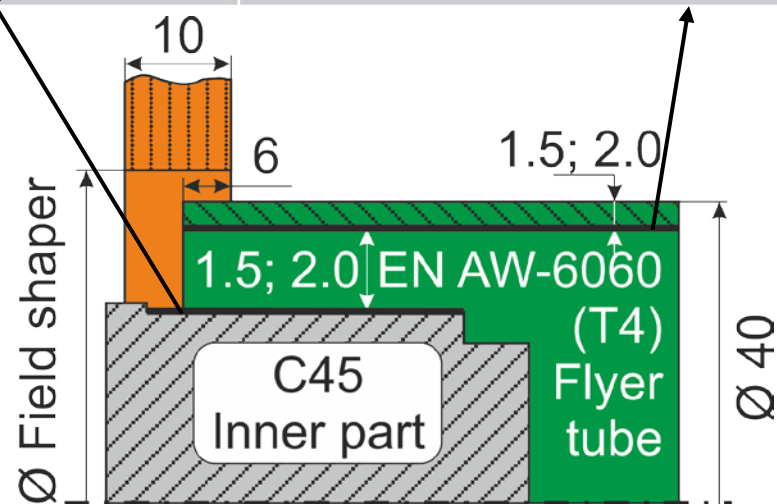
## Process of MPW with tubular parts



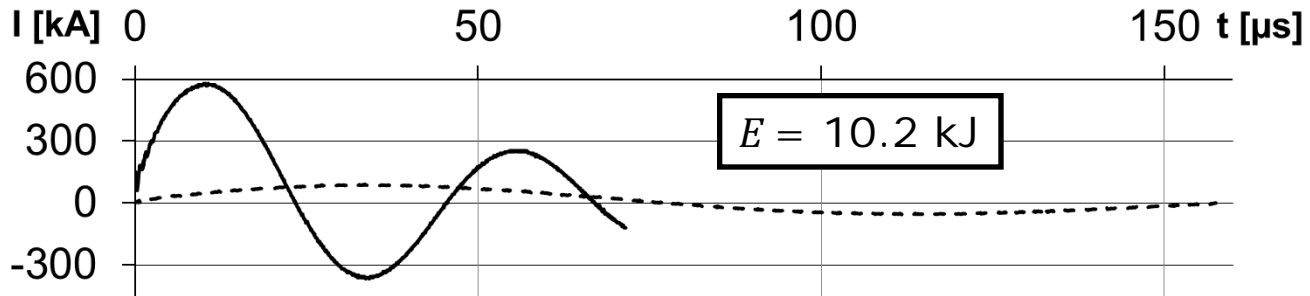
Are typical industrial coatings compatible with magnetic pulse welding?

## 2. Experiments with coatings and results

Inner part	Flyer tube
Electroplating nickel 5 $\mu\text{m}$	Anodized 5 $\mu\text{m}$ , 10 $\mu\text{m}$
Electroplating zinc 5 $\mu\text{m}$ , 10 $\mu\text{m}$	Hard anodized 15 $\mu\text{m}$
Nitrated	Chromated
PVD nickel 2.5 $\mu\text{m}$	Acid passivated
PVD chrome 1.5 $\mu\text{m}$	



## Parameters of pulse stations: Tool coil current $I(t)$

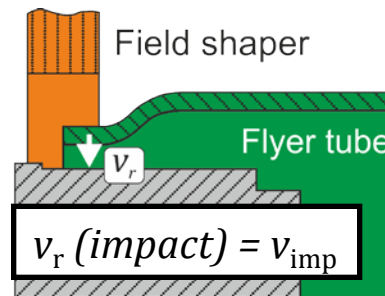


$f \approx 20$  kHz  
 $I_{\max} = 580$  kA  
 $v_{\text{imp}} = (380 \dots 460)$  m/s

$f \approx 7$  kHz  
 $I_{\max} = 86$  kA  
 $v_{\text{imp}} = (240 \dots 260)$  m/s



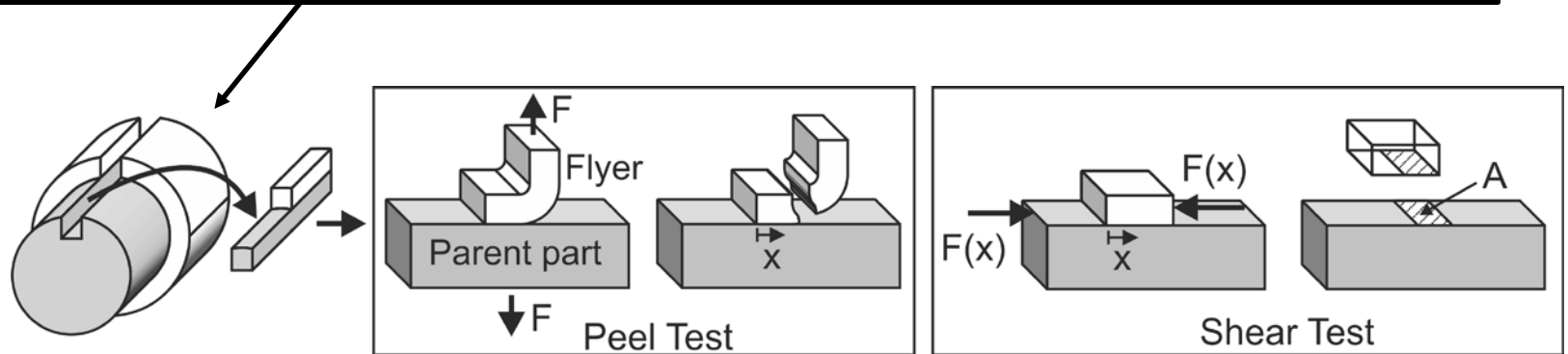
Bmax MPW50/25:  
 single turn coil, integrated  
 $\varnothing$  42 mm field shaper



Maxwell – Magneform 7000:  
 8-turn coil with  $\varnothing$  41 mm  
 field shaper

## Basic results after cutting the flyer tube

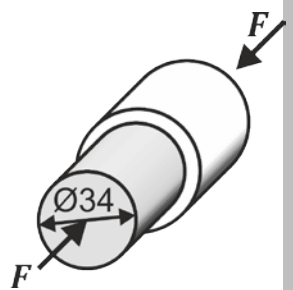
	Inner part	Flyer tube
Not welded	Electroplating zinc 5 & 10 $\mu\text{m}$	Hard anodized 15 $\mu\text{m}$
	Nitrated	Anodized 10 $\mu\text{m}$
Difficult to weld		Anodized 5 $\mu\text{m}$
Welded	Electroplating nickel 5 $\mu\text{m}$	Chromated
	PVD nickel 2.5 $\mu\text{m}$	Acid passivated
	PVD chrome 1.5 $\mu\text{m}$	



## Welding results: Length and strength

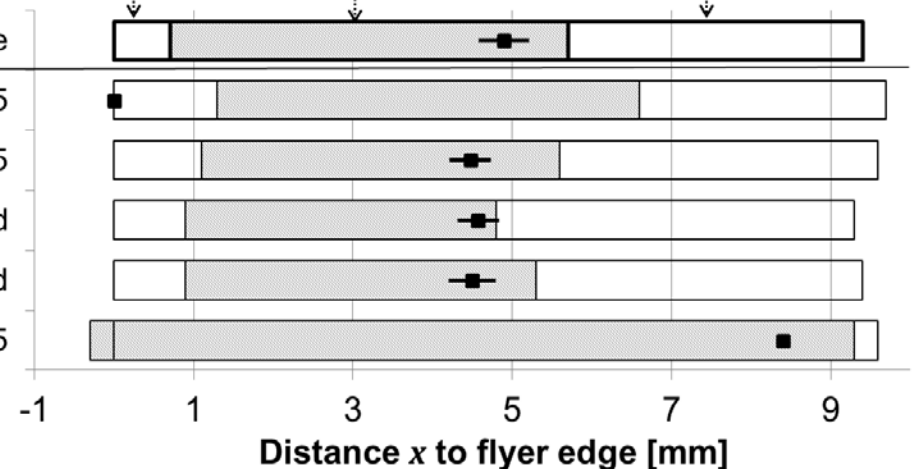
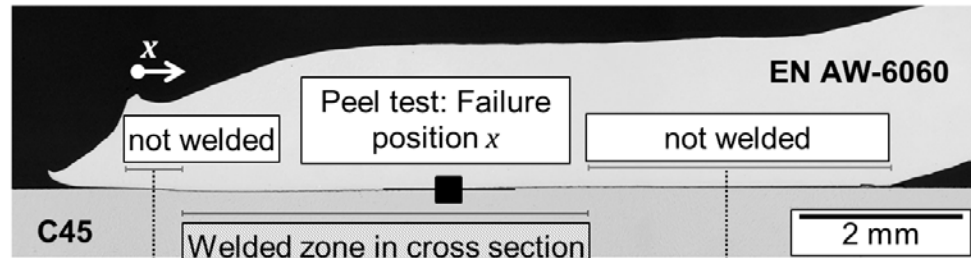
Acceleration gap  $g = 1.5 \text{ mm}$   
 Tube thickness  $t = 1.5 \text{ mm}$   
 Impact velocity  $v_{\text{imp}} \approx 390 \text{ m/s}$

Average maximum load  $F$  for complete part (based on shear test results) [kN]



76  
70  
81  
61  
73  
139

Ref.: St-Pure, Al-Pure  
 St-PVD Ni2.5  
 St-PVD Cr1.5  
 Al-Acid passivated  
 Al-chromated  
 St-Ni5

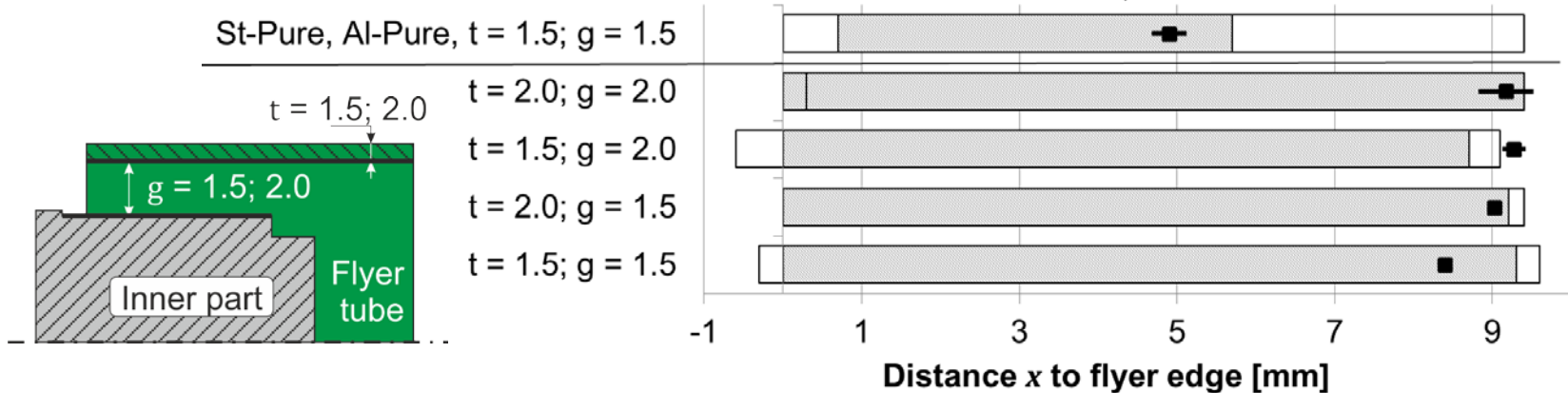
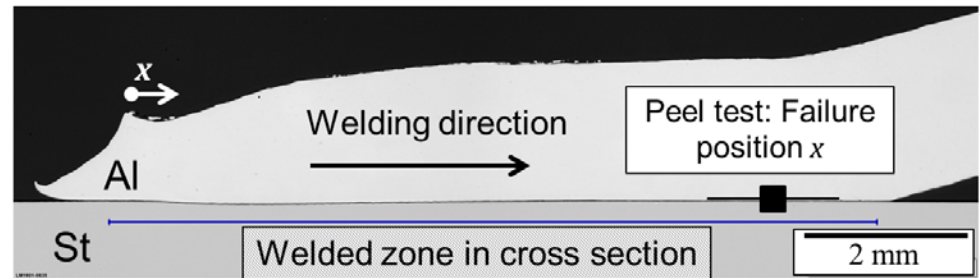


Electroplating nickel 5  $\mu\text{m}$  clearly increases the weld length and the maximum load



# Focus: Electroplating nickel 5 $\mu\text{m}$ in different geometrical configurations

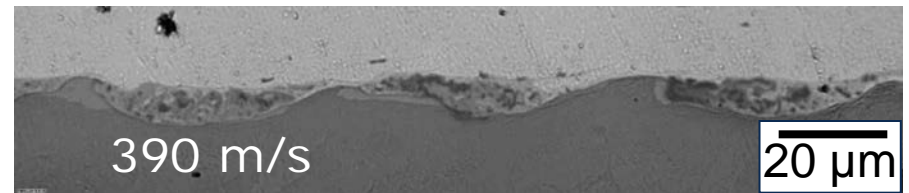
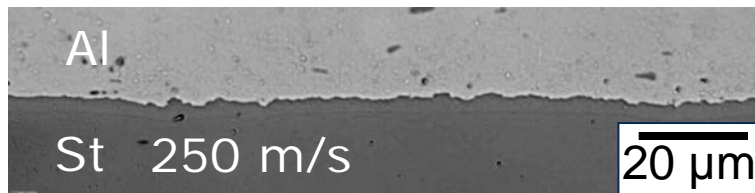
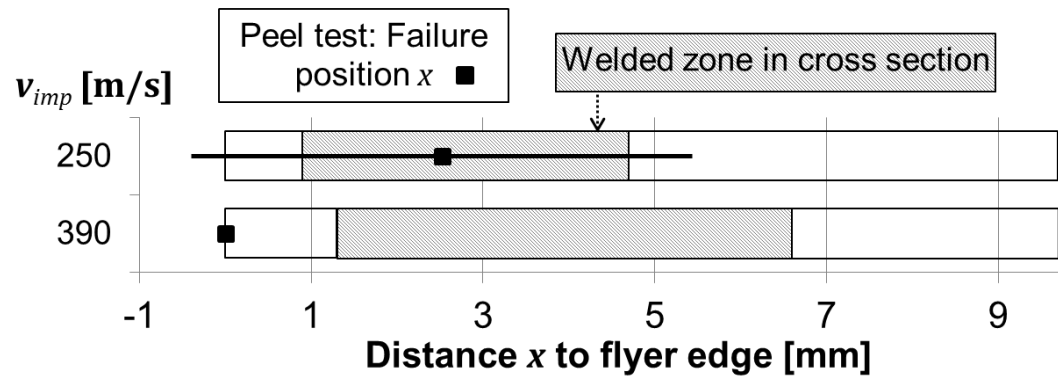
$v_{\text{imp}} \approx (380 \dots 460) \text{ m/s}$



Electroplating Nickel 5  $\mu\text{m}$  increases the weld length during MPW in all tested configurations

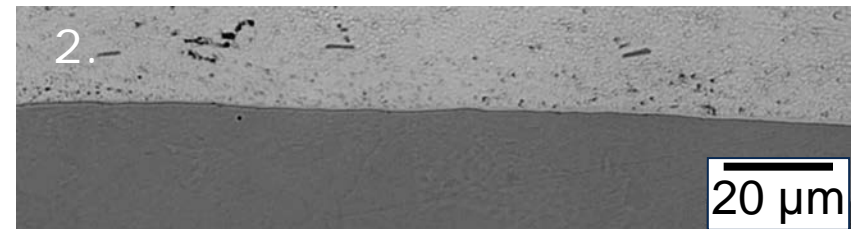
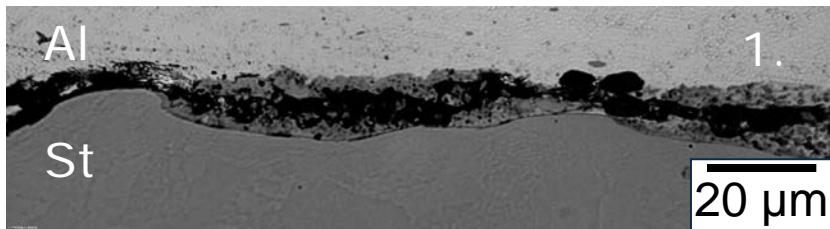
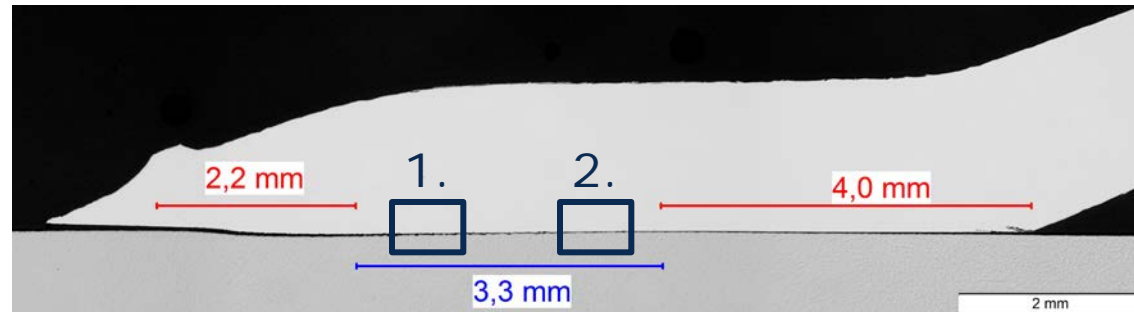
## Focus: Impact velocity

Parameters: PVD Ni  $2.5 \mu\text{m}$ ,  $E = 10.2 \text{ kJ}$ ,  $t = 1.5 \text{ mm}$ ,  $g = 1.5 \text{ mm}$



High impact velocity  $\rightarrow$  wavy interface

## Focus: Anodized aluminum



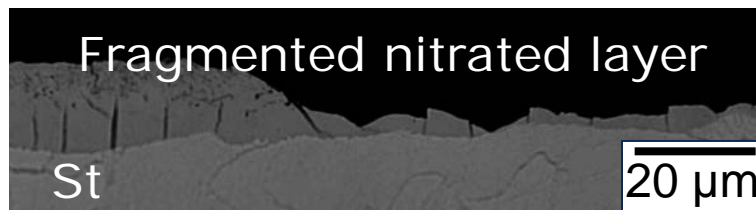
Global deformation of the flyer fractures the anodized layer

1. Before start of jetting: Embedded layer
2. With jetting: Removed layer

### 3. Classification of coatings

#### Type I – Brittle surface coatings

	Inner part	Flyer tube
Coatings	Electroplating zinc 5 & 10 $\mu\text{m}$ Nitrated	Hard anodized 15 $\mu\text{m}$ Anodized 5 & 10 $\mu\text{m}$
Fragmentation	Partly (delaminated)	Strongly
Removable by the jet	Not completely	Completely (Anodized 5 $\mu\text{m}$ )

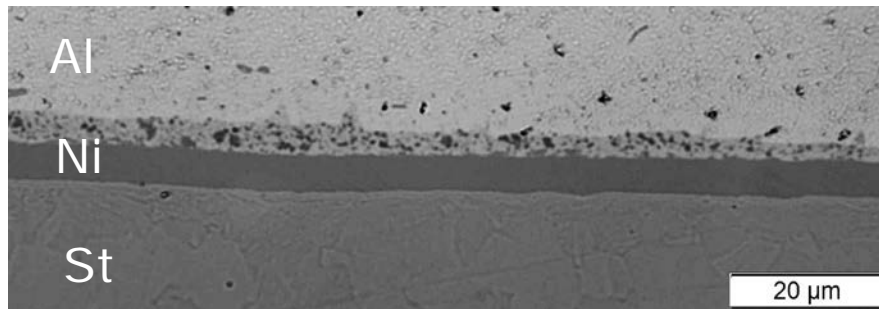
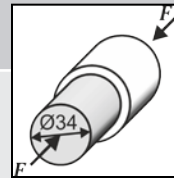


Brittle surface coatings: Weldability depends on the amount of deformation prior jetting

### 3. Classification of coatings

#### Type II – Thick and ductile surface coatings

Coating inner part	Shear strength [MPa]	Average maximum load F for complete part (based on shear test results) [kN]	Weld length [mm]
-	143±8	76	5
Electroplating nickel 5 µm	140±17	139	9,6



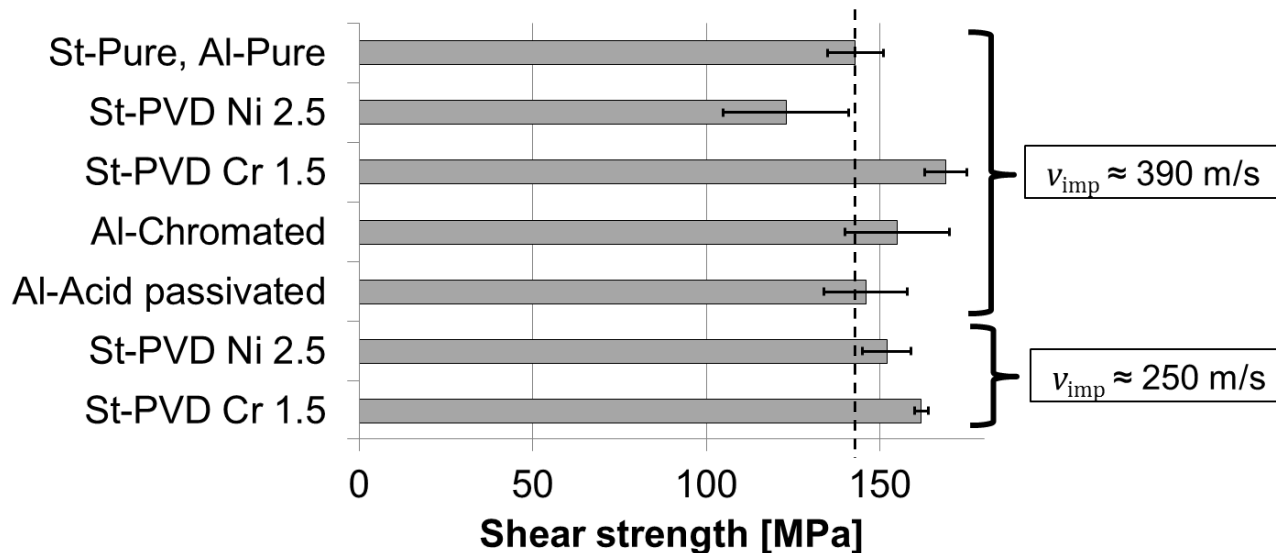
Thickness  $t = 1.5$  mm  
 Gap  $g = 1.5$  mm  
 Energy  $E = 10.2$  kJ  
 Impact velocity  $v_{imp} \approx 390$  m/s

Thick and ductile layers: Increase of weld length and maximum load

### 3. Classification of coatings

#### Type III – Thin and ductile surface coatings

Tube thickness  $t = 1.5 \text{ mm}$ , gap  $g = 1.5 \text{ mm}$ , energy  $E = 10.2 \text{ kJ}$



Thin and ductile layers: Embedding in the weld interface is possible with modified strength

### 3. Classification of coatings – Three types

I. Brittle:

→ unfavorable on the inner part

→ feasible on the flyer tube

II. Thick and ductile:

→ improved weld length and quality

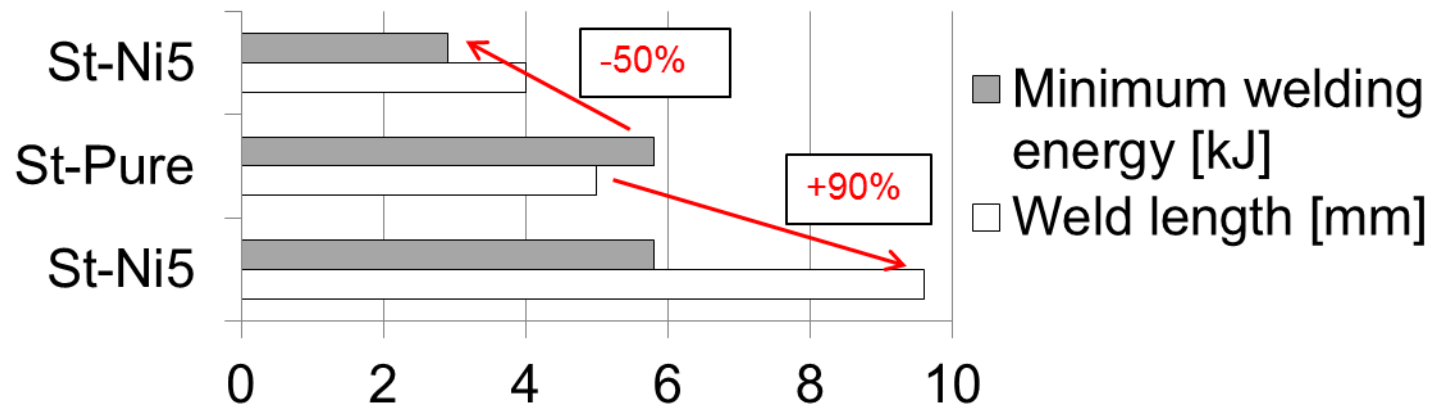
III. Thin and ductile:

→ uncritical for magnetic pulse welding

## 4. Tailored joining: Outlook

For welding of EN AW-6060 to C45, electroplating nickel 5  $\mu\text{m}$  (on steel) can:

- Increase the weld length  $\Leftrightarrow$  decrease the energy



- Lower the necessary impact velocity for welding
- Avoid spallation of already welded areas





## Acknowledgements

- For your interest in magnetic pulse welding
- For the financial support from the German Research Foundation (DFG). This work is based on the results of subproject A1 of the priority program 1640 (“joining by plastic deformation”) in collaboration with Fraunhofer IWS and the Institute of Forming Technology and Lightweight Construction, TU Dortmund University.